

The Metallurgical Examination and Inspection of Apache Tail Rotor Strap Pack Laminates and Assemblies

by Scott M. Grendahl

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Abstract

The U.S. Army Research Laboratory-Weapons and Materials Research Directorate (ARL-WMRD) performed a dimensional inspection and metallurgical investigation of AH-64 Apache tail rotor strap pack assemblies and individual laminate sets. All of the dimensional critical characteristics were examined in an attempt to determine the cause of a buckling phenomenon within the strap pack assemblies. Conformance to the manufacturer's governing specifications with respect to the material, heat treatment, and marking requirements was also investigated. The cause of the buckling was attributed to a combination of factors. Dimensional nonconformances were identified. Most of the hole diameters were found to be well below the specified range, causing the assemblies to be forced together. Transposition of the laminates during manufacture was also highly likely to have occurred, adding to the misalignment of the assembly. All other characteristics of the laminates and assemblies were found to conform to the governing part drawings and specifications.

Acknowledgments

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1. Introduction

The U.S. Army Aviation and Missile Command (AMCOM) requested an investigation consisting of metallurgical examination and dimensional inspection of Apache tail rotor strap pack assemblies and individual laminate sets. The laminate material is very thin (approximately 0.014 in) sheet AM-355, a semiaustenetic stainless steel. The U.S. Army Research Laboratory, Weapons and Materials Research Directorate (ARL-WMRD), received two Quality Deficiency Report (QDR) exhibits, which were to be used as the assemblies for inspection. Additionally, nine individual laminate sets were sent to ARL-WMRD for inspection (serial numbers [SN] 003343-1167, -1168, -1169, -1172, -1173, -1174, -1175, -1176, and -1177). ARL-WMRD was requested to perform a dimensional inspection of the two QDR assemblies per the governing specifications and also verify that they were properly assembled. Additionally, ARL-WMRD was requested to inspect three laminates (selected at random) from each separate laminate set received for conformance to the governing documents. Later, this was altered to include a complete dimensional inspection of one laminate set selected at random. Verification of surface finish, edge finish, and hole finish and all other critical characteristics was to be determined as prescribed by the governing documents. ARL-WMRD was also requested to perform a full metallurgical investigation of one laminate from both QDR assemblies received to verify material and heat treatment. Finally, it was requested of ARL-WMRD to substantiate that all components were marked and designated in accordance with the appropriate specifications.

2. Objectives

The purpose of this work was to determine the cause of the buckling phenomenon on the two QDR tail rotor assembly exhibits. Additionally, all components involved were evaluated for conformance to the governing manufacturing, process, and identification specifications of the assembly.

3. Experimental Procedure

3.1 Visual Inspection and Light Optical Microscopy. Both QDR exhibits (designated W81CL8940027 for SN 003343-0899 and W81CL8940085 for SN 003343-1548) received by ARL-WMRD were visually inspected [1, 2]. It was noted that both exhibits experienced extensive buckling between the individual laminates that make up the assemblies. The assembly is governed by the McDonnell Douglas drawing package BP-7-211421035 [3]. Figures 1 and 2 depict QDR exhibit 003343-1548 (1548) as received by ARL-WMRD.

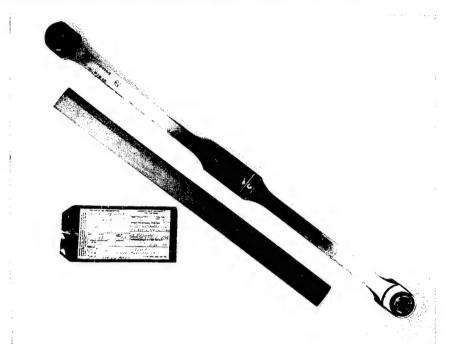


Figure 1. Macrograph of the As-Received Strap Pack 1548 (Top View). (Scale in Inches.)

Figures 3 and 4 show QDR exhibit 003343-0899 (0899) as received by ARL-WMRD. The individual quality deficiency reports designate buckling and/or displacement of the first laminate for exhibit 1548 and the third and eleventh laminate for exhibit 0899. These findings were verified by ARL-WMRD via optical microscopy. The first laminate was visibly buckled on exhibit 1548, as depicted in Figure 5. Closer examination of the white outlined box in Figure 4 reveals the buckling of the third and eleventh laminates on exhibit 0899. The additional nine

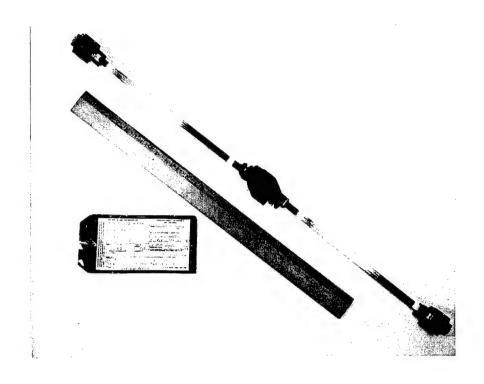


Figure 2. Macrograph of the As-Received Strap Pack 1548 (Side View). (Scale in Inches.)

laminate sets received by ARL-WMRD were also inspected for surface finish and marking requirements per EPB-4-321, Rev. E [4]. All components had surface finishes well within specification. The individual laminates had surface finishes ranging from 2-4 Ra (μm), well within the specified value of 8 Ra (μm). The laminates are governed by the McDonnell Douglas laminate drawing package, BP-7-211421023 and the AM-355 material specification, HMS-6-1073, Rev. E [5, 6]. All tail rotor laminates were blanked within 15° of the longitudinal grain direction of the components in agreement with EPB-4-321, Rev. E [4]. The components were also correctly marked and/or stamped according to the governing identification and serialization specifications, HP 8-5 and HP 8-8 [7, 8].

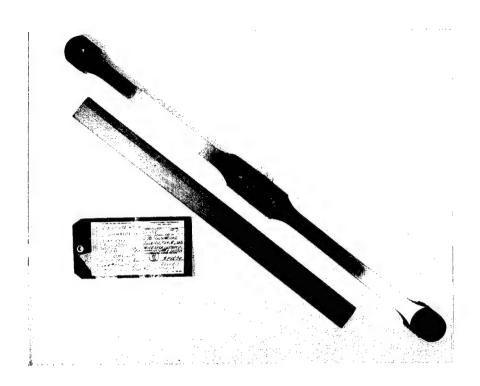


Figure 3. Macrograph of the As-Received Strap Pack 0899 (Top View). (Scale in Inches.)

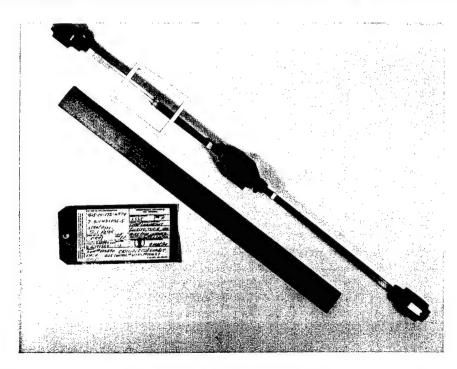


Figure 4. Macrograph of the As-Received Strap Pack 0899 (Side View). (Scale in Inches.)

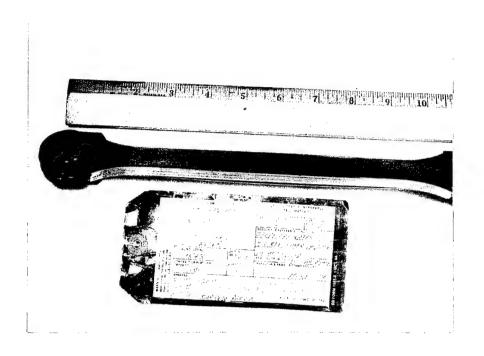


Figure 5. Macrograph of the Buckling on Strap Pack 1548. (Scale in Inches.)

3.2 Dimensional Inspection. A three-axis coordinate measuring machine (CMM) was used to check the dimensional conformity of the strap pack laminates. It must be understood in an analysis of the data that the laminates were edge-finished prior to dimensional inspection. This is significant, since the CMM employs a spherical ruby stylus when acquiring measurement data. If the edges of the laminates are also rounded, slight inaccuracies may exist in the measurements obtained due to the extreme thinness of the laminates (approximately 0.014 in). Figure 6 illustrates this phenomenon. However, it is important to note that this small source of error would not account for hole dimensions with measured value smaller than that specified, as the drawing illustrates. If the spherical stylus caused error to be introduced, the dimensions of the holes would be artificially inflated rather than reduced. Therefore, the slight inaccuracy might only explain dimensions that are out of tolerance by being larger than specified. Dimensions found to be smaller than specified cannot be explained away under this argument and are of significant concern. This inaccuracy in measurement due to the edge finishing and spherical stylus is very small, approximately 0.0005 in maximum, and is exaggerated in Figure 6.

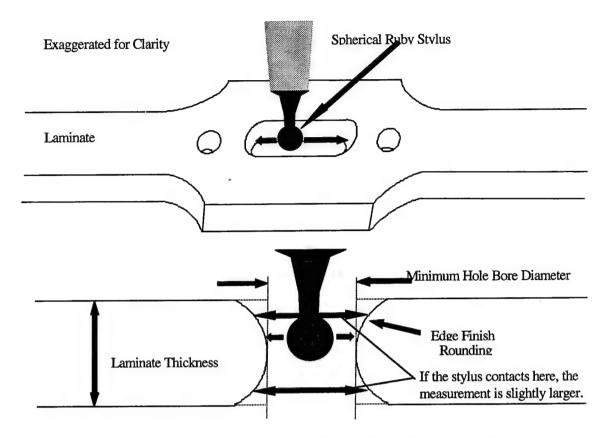


Figure 6. Illustration of the Measurement Inaccuracy Due to Edge Finishing.

Table 1 is a listing of the measurements taken by the CCM during the inspection of the QDR exhibit tail rotor strap pack assemblies, 1548 and 0899. Refer to the laminate illustration, Figure 7, for the individual measurement locations.

4. Discussion

The boxed data in Table 1 indicate the most likely source of the buckling. It can be seen from the data for dimensions E and F that the average value of DIM. E is larger by 0.006 in (average value DIM. E = 1.1294 in and average value DIM. F = 1.1233 in, neglecting the boxed data). The transposition occurs when a laminate is rotated 180° and inserted back into the stack. Therefore, DIM. E becomes DIM. F for the transposed laminate. It can be seen in the data that the transposed laminate's DIM. E values closely resemble the other laminate's DIM. F values.

Table 1. Dimensional Data for QDR Exhibits 1548 and 0899

Laminate	DIM. A	DIM. B	DIM. C	DIM. D	DIM. E	DIM. F	HOLE 1	HOLE 2	HOLE 3	HOLE 4
Specification	23.200	11.600	11.600	2.250	1.125	1.125	0.6883	0.6883	0.1955	0.1955
Tolerance	± 0.010	± 0.010	± 0.010	± 0.010	±0.010	±0.010	+ 0.0002	+ 0.0002	± 0.0005	± 0.0005
							- 0.0003	- 0.0003		
#1548 - 1	23.20456	11.60183	11.60272	2.25099	1.12874	1.12225	0.68314	0.68443	0.19135	0.19213
#1548 - 2	23.20537	11.60260	11.60276	2.25192	1.12187	1.13005	0.68486	0.68523	0.19210	0.19622
#1548 - 3	23.20522	11.60138	11.60384	2.25078	1.11997	1.13080	0.68531	0.68611	0.19266	0.19195
#1548 - 4	23.20614	11.60289	11.60325	2.25194	1.12089	1.13105	0.68582	0.68586	0.19331	0,19233
#1548 - 5	23.20673	11.60381	11.60292	2.25018	1.12116	1.12901	0.68625	0.68350	0.19139	0.19238
#1548 - 6	23.20611	11.60287	11.60324	2.25046	1.11985	1.13062	0.68531	0.68760	0.19168	0.19322
#1548 - 7	23.20587	11.60316	11.60271	2.25145	1.12176	1.12969	0.68687	0.68330	0.19110	0.19196
#1548 - 8	23.20560	11.60240	11.60320	2.25260	1.12170	1.13090	0,68520	0,68500	0.19290	0.19220
#1548 - 9	23.20480	11.60250	11.60230	2.25030	1.12100	1.12930	0,68590	0.68520	0.19470	0.19380
#1548 - 10	23.20700	11.60290	11.60420	2.24930	1.11930	1.12990	0.68630	0.68580	0.19340	0.19300
#1548 - 11	23.20600	11.60310	11.60290	2.25090	1.12210	1.12980	0.68580	0.68600	0.19400	0.19290
#1548 - 12	23.20550	11.60280	11.60260	2.25230	1.12240	1.12990	0.68530	0.68570	0.19290	0.19140
#1548 - 13	23.20590	11.60310	11.60280	2.25130	1.12170	1.12950	0.68710	0.68640	0.19390	0.19390
#1548 - 14	23.20570	11.60310	11.60260	2.25150	1.12120	1.13030	0.68590	0.68570	0.19360	0.19290
#1548 - 15	23.20680	11.60330	11.60350	2.25160	1.12150	1.13010	0.68680	0.68720	0.19480	0.19370
#1548 - 16	23.20570	11.60290	11.60280	2.25070	1.12120	1.12940	0.68570	0.68600	0.19320	0.19320
#1548 - 17	23.20610	11.60290	11.60320	2.25180	1.12190	1.12990	0.68780	0.68800	0.19490	0.19430
#1548 - 18	23.20600	11.60290	11.60320	2.25060	1.12140	1.12990	0.68740	0.68730	0.19440	0.19370
#1548 - 19	23.20620	11.60290	11.60330	2.25180	1.12240	1.12920	0.68740	0.68630	0.19440	0.19340
#1548 - 20	23.20530	11.60250	11.60280	2.25200	1.12150	1.13050	0.68680	0.68570	0.19400	0.19420
#1548 - 21	23.20620	11.60290	11.60330	2.25050	1.12120	1.12930	0.68600	0,68690	0.19310	0.19250
#1548 - 22	23.20570	11.60290	11.60280	2.25120	1.12180	1.12930	0.68540	0.68680	0.19270	0.19210
#0899 -1	23.20560	11.60270	11.60290	2.25170	1.12840	1.12320	0.68770	0.68740	0.19500	0.19470
#0899 - 2	23.20600	11.60290	11.60320	2.25250	1.12940	1.12300	0.68780	0.68760	0.19480	0.19470
#0899 - 3	23.20540	11.60270	11.60260	2.25220	1.12280	1.12940	0.68710	0.68750	0.19630	0.19580
#0899 - 4	23.20560	11.60270	11.60290	2.25190	1.1289	1.12300	0.68710	0.68680	0.19530	0.19500
#0899 - 5	23.20460	11.60210	11.60250	2.25220	1.12860	1.12350	0.68730	0.68730	0.19480	0.19400
#0899 - 6	23.20560	11.60240	11.60320	2.25220	1.12860	1.12360	0.68700	0.68700	0.19540	0.19500
#0899 -7	23.20530	11.60240	11.60290	2.25220	1.12880	1.12350	0.68740	0,68740	0.19530	0.19570
#0899 - 8	23.20550	11.60290	11.60290	2.25280	1.12940	1.12340	0.68710	0.68670	0.19410	0.19460
#0899 - 9	23.20540	11.60260	11.60270	2.25230	1.12920	1.12310	0.68720	0.68760	0.19530	0.19570
#0899 -10	23.20520	11.60250	11.60280	2.25150	1.12880	1.12270	0.68730	0.68730	0.19490	0.19410
#0899 -11	23.20560	11.60280	11.60280	2.25360	1.12300	1.13060	0.68840	0.68840	0.19430	0.19470
#0899 -12	23.20570	11.60290	11.60280	2.25270	1.12950	1.12320	0.68660	0.68660	0.19490	0.19440
#0899 -13	23.20550	11.60250	11.60300	2.25300	1.12960	1.12340	0.68730	0.68720	0.19530	0.19450
#0899 -14	23.20500	11.60250	11.60250	2.25310	1.12940	1.12360	0.68670	0.68660	0.19440	0.19440
#0899 -15	23.20520	11.60260	11.60260	2.25310	1.12950	1.12350	0.68730	0.68630	0.19470	0.19420
#0899 -16	23.20500	11.60250	11.60250	2.25280	1.12960	1.12330	0.68790	0.68740	0.19500	0.19540
#0899 -17	23.20560	11.60270	11.60290	2.25340	1.12990	1.12350	0,68720	0.68730	0.19470	0.19520
#0899 -18	23.20590	11.60310	11.60280	2.25340	1.12970	1.12370	0.68660	0.68710	0.19470	0.19440
#0899 -19	23.20550	11.60270	11.60280	2.25350	1.12980	1.12380	0.68680	0.68690	0.19390	0.19420
#0899 - 20	23.20510	11.60240	11.60270	2.25370	1.13000	1.12380	0.68660	0.68660	0.19400	0.19400
#0899 - 21	23.20550	11.60280	11.60270	2.25350	1.13120	1.12230	0.68680	0.68660	0.19400	0.19470
#0899 - 22	23.20520	11.60250	11.60260	2.25320	1.12970	1.12340	0.68690	0.68710	0.19430	0.19450

Note: Boxed data indicate a transposition of the laminate about the y-axis. Shaded data indicate values out of specification.

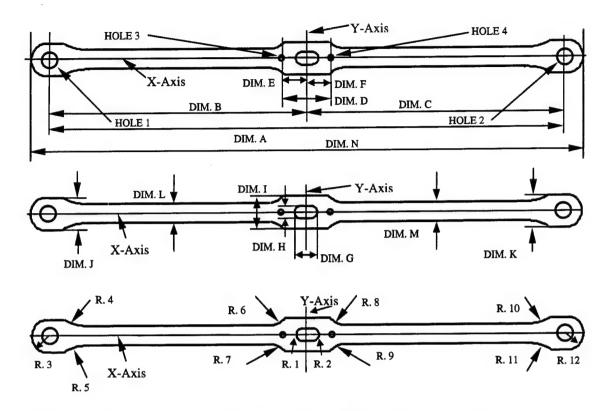


Figure 7. Illustration of the Defined Laminate Dimensions for Tables 1, 2, 3, and 4.

The converse also holds true. Once a 180° transposition about the Y-axis of a laminate has occurred, forcing a rivet through these centrally located rivet holes will cause an offset of the entire laminate. Therefore, the assembly is forced to buckle when the bushings are placed through the ends of the laminate stack. Figure 8 visually depicts the transposition and buckling scenario.

Further evidence of this scenario is suggested by the displacement/buckling location within the laminate stack as reported previously. The displacement and buckling location matches precisely with the boxed data laminate numbers in Table 1. In strap pack 1548, the first laminate is visibly displaced (refer to Figure 5), and for strap pack 0899, the third and eleventh laminates are displaced (refer to Figure 4).

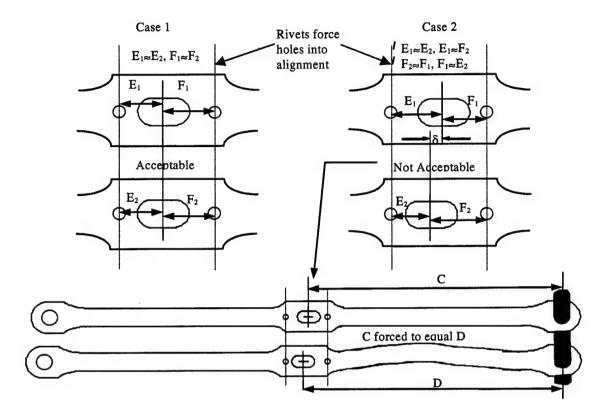


Figure 8. Illustration of the Transposition About the Y-Axis and Buckling Scenario.

Based upon these initial findings of the QDR exhibits, ARL-WMRD was asked to perform a full dimensional analysis of three randomly selected laminates from each of the nine individual laminate sets received, in addition to two single separate laminates. Tables 2–4 list the data acquired using the CMM.

The only significant finding in the data in Table 2 was that the first extra laminate inspected was considerably out of tolerance with respect to its width dimensions. The transposition event is not discernable within this data due to the absence of the data from the complete sets. Three laminates are not enough to establish a pattern in the measurement data.

Based upon the findings in Table 3, it was obvious that a complete laminate set must be dimensionally checked for the transposition about the Y-axis to be seen within a laminate set.

Table 2. Dimensional Data for Randomly Selected Individual Laminate Sets and Odd Laminates

DIM. N	24.840	REF.	24.8555	24.8534	24.8491	24.8482	24.8497	24.8541	24.8569	24.8521	24.8546	24.8569	24.8505	24.8549	24.8536	24.8569	24.8582	24.8586	24.8510	24.8547	24.8505	24.8525	24.8563	24.8569	24.8545	24.8534	24.8526	24.8483	24.8476	24.9166	248574
DIM. M	0.790	± 0.010	0.7924	0.7922	0.7922	9062.0	0.7921	0.7927	0.7910	0.7914	0.7925	0.7921	0.7939	0.7947	0.7915	0.7921	0.7922	0.7933	0.7929	0.7928	0.7919	0.7930	0.7923	0.7934	0.7934	0.7911	0.7913	0.7926	0.7912	0.8525	0 7964
DIM. L	0.790	± 0.010	0.7922	0.7932	0.7922	9062.0	0.7921	0.7927	0.7927	0.7910	0.7914	0.7921	0.7939	0.7947	0.7915	0.7921	0.7922	0.7933	0.7929	0.7928	0.7919	0.7930	0.7923	0.7934	0.7934	0.7911	0.7913	0.7916	0.7928	0.8495	0.7980
DIM. K	1.550	± 0.010	1.5569	1.5582	1.5571	1.5550	1.5562	1.5572	1.5545	1.5555	1.5572	1.5555	1.5578	1.5581	1.5561	1.5569	1.5577	1.5566	1.5571	1.5569	1.5554	1.5569	1.5576	1.5572	1.5567	1.5557	1.5567	1.5566	1.5561	73 191	1 5578
DIM. J	1.550	± 0.010	1.5572	1.5579	1.5570	1.5549	1.5561	1.5573	1.5556	1.5566	1.5570	1.5555	1.5566	1.5576	1.5567	1.5566	1.5571	1.5565	1.5561	1.5571	1.5559	1.5575	1.5568	1.5570	1.5570	1.5552	1.5566	1.5551	1.5561	1.6125	1 5599
DIM. I	1.550	± 0.010	1.5568	1.5567	1.5570	1.5539	1.5533	1.5535	1.5539	1.5541	1.5545	1.5537	1.5556	1.5552	1.5512	1.5533	1.5541	1.5548	1.5553	1.5560	1.5546	1.5546	1.5548	1.5568	1.5570	1.5555	1.5565	1.5574	1.5569	1.6145	1 5679
DIM. H	099'0	± 0.010	0.6635	0.6622	0.6637	0.6641	0.6649	0.6635	0.6640	0.6634	0.6637	0.6636	0.6650	0.6644	0.6656	0.6645	0.6642	0.6651	0.6657	0.6644	0.6644	0.6653	0.6644	0.6640	0.6630	0.6633	0.6640	0.6646	0.6656	0.6641	0.6631
DIM. G	1.100	± 0.010	1.1042	1.1029	1.1031	1.1033	1.1028	1.1028	1.1026	1.1037	1.1030	1.1040	1.1020	1.1021	1.1036	1.1038	1.1029	1.1034	1.1057	1.1052	1.1050	1.1047	1.1040	1.1041	1.1037	1.1040	1.1043	1.1044	1.1060	1.1090	1,1072
DIM. F	1.125	± 0.010	1.1266	1.1259	1.1260	1.1267	1.1251	1.1267	1.1252	1.1250	1.1246	1.1253	1.1254	1.1243	1.1266	1.1250	1.1255	1.1266	1.1256	1.1260	1.1260	1.1266	1.1263	1.1246	1.1251	1.1245	1.1265	1.1249	1.1240	1.1287	1.1231
DIM. E	1.125	± 0.010	1.1261	1.1263	1.1262	1.1259	1.1282	1.1267	1.1259	1.1261	1.1265	1.1266	1.1269	1.1275	1.1261	1.1264	1.1265	1.1250	1.1246	1.1248	1.1248	1.1247	1.1241	1.1273	1.1269	1.1270	1.1252	1.1263	1.1265	1.1223	1 1 1 2 8 1
DIM. D	2.250	± 0.010	2.2527	2.2522	2.2523	2.2526	2.2533	2.2534	2.2511	2.2511	2.2510	2.2519	2.2523	2.2518	2.2515	2.2514	2.2520	2.2515	2.2502	2.2507	2.2508	2.2512	2.2503	2.2519	2.2520	2.2515	2.2517	2.2512	2.2505	2.2510	22512
DIM. C	11.600	± 0.010	11.6004	11.6003	11.6002	11.6002	11.5991	11.6003	11.6003	11.6002	11.6001	11.6004	11.6003	11.6003	11.6004	11.6004	11.6002	11.6007	11.6005	11.6008	11.6004	11.6010	11.6009	11.6004	11.6002	11.6002	11.6003	11.6001	11.6001	11.6030	11 6029
DIM. B	11.600	± 0.010	11.6004	11.6003	11.6002	11.6002	11.5991	11.6003	11.6003	11.6002	11.6001	11.6004	11.6003	11.6003	11.6004	11.6004	11.6002	11.6007	11.6005	11.6008	11.6004	11.6010	11.6009	11.6004	11.6002	11.6002	11.6003	11.6001	11.6001	11.6030	11 6029
DIM. A	23.200	± 0.010	23.2009	23.2007	23.2005	23.2005	23.1982	23.2007	23.2007	23.2004	23.2002	23.2008	23.2006	23.2007	23.2009	23.2009	23.2004	23.2015	23.2011	23.2017	23.2009	23.2021	23.2018	23.2009	23.2004	23.2005	23.2007	23.2003	23.2003	23.2060	23,2058
Laminate	Specification	Tolerance	1172 - 7	1172 - 16	1172 - 21	1173 - 2	1173 - 9	1173 - 19	1167 - 1	1167 - 8	1167 - 20	1169 - 2	1169 - 13	1169 - 22	1168 - 2	1168 - 12	1168 - 20	1174 - 4	1174 - 11	1174 - 20	1175 - 1	1175 - 12	1175 - 19	1176 - 3	1176 - 10	1176 - 21	1177 - 5	1177 - 11	1177 - 17	Extra #1	Extra #2

Note: Shaded data indicate a value out of specification.

Table 3. Dimensional Data for the Holes and Radii of Randomly Selected Laminates

Laminate	Hole 1	Hole 2	Hole 3	Hole 4	Rad. 3	Rad. 4	Rad. 5	Rad. 6	Rad. 7	Rad. 8	Rad. 9	Rad. 10	Rad. 11	Rad. 12
Specification Tolerance	0.6883 + 0.0002 - 0.0003	0.6883 + 0.0002 - 0.0003	0.1955 ± 0.0005	0.1955 ± 0.0005	0.82 ± 0.03	2.00 ± 0.03	0.82 ± 0.03							
1172 - 7	97890	17890	0.1941	0.1940	0.8270	1.9290	1.9626	2.0030	1.9692	1.8446	1.8539	1.9981	1.9854	0.8276
1172 - 16	8989'0	0.6866	0.1944	0.1942	0.8244	2.0484	1.8565	1.9534	1.9709	1 9519	1 9043	67061	1.9606	0.8283
1172 - 21	0.6872	0.6868	0.1938	0.1944	0.8247	2.0259	1.8329	1.8933	1.9754	1.888.4	01061	1.8360	2.0176	0.8239
1173 - 2	0.6874	0.6869	0.1922	0.1941	0.8226	1.9733	1 7778	2.0883	1.9952	2.0374	19157	1 9600	2.0074	0.8251
1173-9	0.6829	0.6871	0.1937	0,1941	0.8258	50961	1.8843	1.9941	1.9497	16131	1.9541	1.9042	1.9354	0.8257
1173 - 19	0.6874	0.6866	0.1942	0.1942	0.8254	2.0131	2.1237	1,9602	1.9923	1.9126	18781	1.8790	2.0036	0.8253
1167 - 1	0.6873	0.6872		0.1942	0.8291	2.0871	2.0342	1.9137	1.9892	2,1128	1.9768	2.0107	1.9742	0.8270
1167 - 8	0.6877	0.6875		0.1943	0.8250	1.9683	2.0187	1.9850	2.0251	2.0125	1.9752	1.9662	2.0049	0.8267
1167 - 20	0.6878	0.6877	0.1947	0.1949	0.8269	1.8214	1.8887	1,9344	2.6394	2.0157	2.0227	1.9634	1.9666	0.8275
1169 - 2	0.6874	0.6869	0.1930	0.1941	0.8298	1.9752	1.9645	1.9998	1.9574	2.0285	1.8977	2.0209	1.9634	0.8263
1169 - 13	89890	0.6865	0.1928	0.1939	0.8243	2.0019	1.8545	85961	1.9964	1.8848	1.8622	1.9823	1.9772	0.8256
1169 - 22	0.6876	0.6873		0.1932	0.8293	1 9515	1,9164	1 9305	16861	1.8502	1.8860	1.9524	16761	0.8249
1168 - 2	0.6876	0.6869	0.1947	0.1944	0.8262	1,9409	1.8675	1.9612	2.0046	1.9869	1.9440	1.9150	1.9976	0.8265
1168 - 12	9,6872	0.6878	0.1943	0.1941	0.8264	2.0093	1.8277	1.9816	1.9938	86967	1.9213	1.9549	1.9989	0.8296
1168 - 20	0.6877	0.6868	0.1942	0.1941	0.8306	1.9896	1 9602	1,9614	2.0111	1.9938	1.9131	1.8419	1.9830	0.8272
1174 - 4	0.6871	0.6873	0.1945	0.1939	0.8308	1.9845	1.9764	1 9378	1.9965	1.9691	1,8404	1.8854	1.9940	0.8263
1174 - 11	0.6878	0.6874	97610	0.1945	0.8262	2.0329	1.8427	1.9972	1.9932	1.9673	1.9593	1.9449	1.9822	0.8237
1174 - 20	0.6873	0.6870	0.1935	0.1941	0.8270	19331	1 8613	1.9042	1.9365	2,0350	1.8910	1.9486	1.9658	0.8260
1175 - 1	0.6863	\$1890	0.1948	0.1947	0.8257	1.8775	1.9290	66961	1,9482	2.0053	1.9175	1.9006	1.9907	0.8239
1175 - 12	0.6871	0.6873		0.1944	0.8235	2.0131	1.8561	1.8926	1.9780	2.0203	1.9513	1.9262	1.9812	0.8269
1175 - 19	0.6870	0.6871	0.1943	0.1936	0.8260	1,9234	1.8671	2.0540	1.9908	1.9741	1.8698	2.0340	2.0055	0.8285
1176 - 3	0.6882	0.6881	0.1948	0.1947	0.8277	1.9827	2.0540	1.8037	2.0052	1.9236	1,97,34	2.0219	2.0085	0.8283
1176 - 10	0.6871	0.6871		0.1936	0.805	2.0038	2.0969	1 9254	2.0123	1.9922	1.8580	1.8446	2.0432	0.8236
1176 - 21	0.6873	0.6865	0.1932	0.1935	0.8243	2.0758	1.6509	1.9837	1.9400	1.9477	1.9817	1.9098	1.9746	0.8286
1177 - 5	0.6876	0.6863		0.1937	0.8250	1,9244	2,0392	1.9729	1.9815	8/16/1	1.9123	1.8865	1.9592	0.8269
1177 - 11	0.6871	0.6876	0.1941	0.1942	0.8231	1.9437	1.9414	1.9728	2.0209	1.9946	1 9038	1.9012	1.9868	0.8249
1177 - 17	0.6872	0.6867	0.1939	6161'0	0.8240	1.9174	1.9714	1.9568	1.9662	1.9504	1.8684	1.9497	2.0015	0.8233
Extra #1	0.6849	0.6864	0.1934	0.1939	0.8535	1.9737	1.9599	2.0032	1.8058	1.9664	1.9715	1.9674	1.9464	0.8571
Extra #2	0.6872	0.6867	0,1931	0.1935	0.8242	1.9839	2.0143	1.9860	1.9847	1.9881	1.9779	1.9673	1.9788	0.8274

Note: Shaded data indicates a value out of specification.

Table 4. Dimensional Examination of Laminate Set 1174

DIM. N	24.840	REF.	24.8483	24.8500	24.8561	24.8568	24.8519	24.8512	24.8440	24.8481	24.8559	24.8534	24.8440	24.8561	24.8486	24.8507	24.8589	24.8457	24.8544	24.8524	24.8462	24.8413	24.8536	24.8494	Rad. 12	0.82	• 0.03	0.8248	0.8237	0.8295	0.8263	0.8374	0.8226
DIM. M	0.790	± 0.010	0.7912	0.7922	0.7908	0.8221	0.7914	0.7904	0.7883	0.7905	0.7914	0.7905	0.7923	0.7893	0.7908	0.7924	0.7947	0.7917	0.7923	0.7915	0.7928	0.7921	0.7936	0.7921	Rad. 11	2.00	• 0.03	2.0028	1.9775	1.9754	1.9638	2.0006	2.0018
Н		4				Н	Н	Н			0.7908			0.7925	0.7913	0.7915	0.7910	0.7923	0.7903	0.7913	\dashv	0.7915	0.7929	0.7916	Rad. 10	2.00	• 0.03	1.8864	1.9246	1,7209	1.8746	2.0432	1.8596
K DIM. L	0.790	0 ± 0.010	Н	3 0.7907	0.7909	4 0.7902	4 0.7912	3 0.7902	3 0.7901	2 0.7901	Н	3 0.7907	5 0.7897	Н	Н	Н	Н	Н			-	Н	Н	Н	Rad. 9	2.00	• 0.03	1,9280	1.9233	90861	1,9076	1.8587	1.8843
DIM. K	1.550	± 0.010	1.5560	1.5543	1.5561	1.5564	1.5574	1.5563	1.5553	1.5572	1.5576	1.5583	1.5575	1.5577	1.5563	1.5577	1.5580	1.5582	1.5570	1.5569	1.5569	1.5582	1.5568	1.5563	Rad. 8	2.00	• 0.03	1.8808	1.9696	89-961	1.9697	1.8771	1.9914
DIM. J	1.550	± 0.010	1.5564	1.5555	1.5572	1.5559	1.5573	1.5554	1.5571	1.5509	1.5566	1.5578	1.5563	1.5578	1.5578	1.5547	1.5582	1.5575	1.5576	1.5569	1.5580	1.5579	1.5576	1.5578	Rad. 7	2.00	• 0.03	1,9559	1,9603	2.0025	1.8002	1.9731	1.9894
DIM. I	1.550	±0.010	1.5544	1.5532	1.5567	1.5549	1.5557	1.5554	1.5549	1.5563	1.5558	1.5567	1.5559	1.5564	1.5559	1.5568	1.5569	1.5567	1.5569	1.5557	1.5566	1.5565	1.5561	1.5567	Rad. 6	2.00	• 0.03	1.9245	1.9274	1.8962	1.9239	1.8988	2.0130
DIM. H	0.660	± 0.010	0.6635	0.6653	0.6608	0.6657	0.6635	0.6641	0.6662	0.6643	0.6646	0.6636	0.6655	0.6646	0.6649	0.6637	0.6643	0.6643	0.6649	0.6648	0.6635	0.6641	0.6639	0.6652	Rad. 5	2.00	• 0.03	1.9626	1.8944	1.9481	1.7876	1.8665	1.9834
DIM. G	1.100	± 0.010	1.1053	1.1061	1.1058	1.1063	1.1057	1.1052	1.1059	1.1054	1.1050	1.1042	1.1055	1.1046	1.1057	1.1050	1.1048	1.1038	1.1052	1.1053	1.1042	1.1034	1.1044	1.1041	Rad. 4		• 0.03	5 1.9778	1,9669	1.9651	1.9844	2.0348	1.9737
DIM. F	1.125	±0.010	1.1263	1.1262	1.1264	1.1266	1.1263	1.1263	1.1261	1.1257	1.1257	1.1258	1.1256	1.1252	1.1250	1.1250	1.1253	1.1240	1.1258	1.1263	1.1254	1.1259	1.1255	1.1258	2 Rad. 3	_	3 • 0.03	5 0.8226	7 0.8248	7 0.8255	7 0.8239	8 0.8226	5 0.8199
H	L	_	\vdash	H		Н		Н	\vdash		H		Н	_	L	\vdash	H	_	_	Н			Н	Н	Rad. 2	0.33	• 0.03	0.3305	6 0.3307	5 0.3307	0.3287	0.3298	5 0.3295
DIM. E	1.125	±0.010	1.1249	1.1246	1.1245	1.1254	1.1248	1.1249	1.1247	1.1254	1.1253	1.1251	1.1248	1.1264	1.1259	1.1260	1.1262	1.1270	1.1247	1.1249	1.1256	1.1248	1.1252	1.1248	Rad. 1	0.33	• 0.03	0.3289	0.3296	0.3295	0.3292	0.3310	0.3295
DIM. D	2.250	± 0.010	2.2513	2.2508	2.2508	2.2517	2.2511	2.2513	2.2507	2.2512	2.2511	2.2509	2.2504	2.2516	2.2509	2.2510	2.2514	2.2506	2.2505	2.2513	2.2510	2.2507	2.2507	2.2507	Hole 4	0.1955	• 0.0005	0.1942	0.1950	0.1950	0.1935	0.1946	0.1946
DIM. C	11.600	± 0.010	11.6005	11.6007	11.6005	11.6009	11.6008	11.6006	11.6007	11.6008	11.6006	11.6007	11.6004	11.6008	11.6005	11.6005	11.6005	11,5893	11.6004	11.6001	11.6004	11.6004	11.6011	11.6004	Hole 3	0.1955	• 0.0005	0.1938	0.1946	97610	0.1938	0.1953	0.1941
DIM. B	11.600	± 0.010	11.6005	11.6007	11.6005	11.6009	11.6008	11.6006	11.6007	11.6008	11.6006	11.6007	11.6004	11.6008	11.6005	11.6005	11.6005	11.5891	11.6004	11.6001	11.6004	11.6004	11.6011	11.6004	Hole 2	0.6883	+ 0.0002	0.6869	0.6877	9/89/0	0.6868	0.6872	0.6876
DIM. A	23.200	± 0.010	23.2001	23.2014	23.2011	23.2018	23.2017	23.2012	23.2015	23.2016	23.2013	23.2014	23.2009	23.2017	23.2011	23.2011	23.2011	23.1966	23.2008	23.2002	23.2008	23.2009	23.2023	23.2008	Hole 1	0.6883	+ 0.0002	0.6871	11890	0.6873	0.6871	6,6865	0.6875
Laminate	Specification	Tolerance	1174-1	1174-2	1174-3	1174-4	1174-5	1174-6	1174-7	1174-8	1174-9	1174-10	1174-11	1174-12	1174-13	1174-14	1174-15	1174-16	1174-17	1174-18	1174-19	1174-20	1174-21	1174-22	Laminate	Specification	Tolerance	1174-1	1174-2	1174-4	1174-5	1174-6	1174-7

Note: Shaded data indicates values out of specification.

Table 4. Dimensional Examination of Laminate Set 1174 (continued)

			Г														
Rad. 12	0.82	• 0.03	0.8241	0.8278	0.8262	0.8191	0.8283	0.8236	0.8268	0.8253	0.8280	0.8262	0.8259	0.8227	0.8228	0.8243	0.8257
Rad. 11	2.00	• 0.03	1.9687	2.0004	2.0209	1,4613	2.0327	2.0155	1'96'1	1.9854	1.9814	1.8559	2.0013	1.9963	1.9854	2.0193	20702
Rad. 10	2.00	• 0.03	1.8724	1,9371	1.8917	1.9543	1 9082	1 8245	89981	1.9814	1.53.28	1.9128	1.9621	1.9404	1.9313	1 9259	1.8488
Rad. 9	2.00	• 0.03	1.8789	1 8644	8055 [19061	1.9818	81/61	66161	2.0639	1.9248	19124	5896-1	1.9864	1.8490	2.0349	1.9446
Rad. 8	2.00	• 0.03	1.9482	18681	97961	1.9881	1 9612	££96 I	1.9420	1 9908	1.9309	1.8908	1 9574	00961	1.9945	11261	1.9857
Rad. 7	2.00	• 0.03	1,8591	1.9781	19261	1.9799	1.9882	1.9630	1.9843	1.9573	1.9984	2.0244	1.9455	1.9524	1.9688	1.9148	1666.1
Rad. 6	2.00	• 0.03	1.9019	1.9858	1.8952	1.9821	1.7965	1.9636	1.8897	1.9554	6956-1	1.8415	1.9520	1,999	1.9526	1.9882	66681
Rad. 5	2.00	• 0.03	1.9277	2.0757	19761	1.8954	1,9014	2.0271	1.8107	1,8559	87 16 1	2.0025	1 9260	88961	1.9381	1,9032	1.7793
Rad. 4	2.00	• 0.03	1.9471	1.9584	1.9833	20196	1.9296	1.9127	2.0057	1.9796	2.0155	1.9687	1.9597	1986	2.0006	1.9386	1.9479
Rad. 3	0.82	• 0.03	0.8224	0.8268	0.8259	0.8240	0.8272	0.8239	0.8228	0.8325	0.8211	0.8273	0.8263	0.8266	0.8176	0.8236	0.8269
Rad. 2	0.33	• 0.03	0.3293	0.3287	0.3295	0.3295	0.3257	0.3307	0.3287	0.3287	0.3289	0.3292	0.3204	0.3221	0.3310	0.3257	0.3309
Rad. 1	0.33	• 0.03	0.3283	0.3329	0.3297	0.3292	0.3298	0.3289	0.3287	0.3287	0.3298	0.3290	0.3296	0.3292	0.3298	0.3296	0.3304 0.3309 0.8269
Hole 4	0.1955	• 0.0005	0.1941	0#610	8561.0	0.1941	0.1943	0.1954	0.1936	0.1934	0 1941	1161.0	0.1952	040	1161.0	0.1943	0.1942
Hole 3	0.1955	• 0.0005	0.1939	0.1942	0.1935	0.1947	0.1945	0.1948	0.1937	8161.0	8:61:0	0.1945	0.1948	6.1939	61610	0.1942	0.1942
Hole 2	0.6883	+ 0.0002	0.6871	698970	0.6871	LL89'0	0.6871	0.6879	0.6867	0.6870	0.6872	0.6875	0.6872	0.6872	6989.0	0.6871	69890
Hole 1	0.6883	+ 0.0002	0.6870	0,6869	0.6865	0.6876	0.6872	0.6883	0.6869	698910	0.6826	0.6872	0.6883	0.6873	0.6867	0.6873	0.6872
Laminate	Specification	Tolerance	1174-8	1174-9	1174-10	1174-11	1174-12	1174-13	1174-14	1174-15	1174-16	1174-17	1174-18	1174-19	1174-20	1174-21	1174-22

Note: Shaded data indicates values out of specification.

Therefore, one complete laminate set (SN 003343-1174, laminates 1–22) was dimensionally checked for conformance to the governing drawings. The results are listed in Table 4. Also, it was acutely apparent from the randomly selected laminates that a problem existed with the hole dimensions. The radii also appeared to be out of specification; however, the edge finishing of the laminates might be effecting these results as previously discussed. Regardless, the hole dimensions are much more critical from a stress analysis standpoint than the radii dimensions.

A 180° transposition about the Y-axis was not seen for any laminate within this laminate assembly set. It cannot be inferred from this investigation that the transposition of the laminates is either an abundant or infrequent occurrence. ARL-WMRD looked at only one complete laminate set, other than the QDR exhibits. A proper estimation of the frequency of this occurrence should be drawn from a larger population of laminate sets. However, the frequency with which the hole dimensions are out of specification (smaller than the acceptable value) is significant and distressing. Considering the hole diameters were found to be smaller than the acceptable values, the bushings and rivets must have been forced through these holes during The bushings and rivets are governed by specifications BP-7-211421028 and NAS-529, respectively [9, 10]. Forcing the rivets through small holes would place undo stresses on the edges of the hole as well as the bushings and rivets. If the bushings and rivets must be forced in place, it could contribute to the buckling condition based on the assumption that the hole tolerances were probably set to allow for imperfections in part symmetry. If the holes are too small, individual laminates are forced to positions that may or may not align with the other laminates. This concept is depicted in Figure 8. In addition, creating stress concentrations on the inner diameters of these holes as well as the bushings and rivets might lead to serious problems for parts under fatigue loading conditions.

The laminates were also checked for conformance with EPB-4-321. No discrepancies or nonconformances with the specification were found. The surface finishes were all within 2–4 Ra, which was well within the specified 8 Ra. Appendices A–D present the data acquired on the edge finishing for the individual laminates of the sets analyzed. Strap packs 0899 and 1548, were examined, in addition to the three randomly selected laminates from each laminate set, the

two extra laminates, and the one complete laminate set 1174. The data were acquired from an image analysis system equipped with a CCD camera. The values obtained are based on a calibration performed on the laminates and are accurate only to one decimal place. The interior hole edge finishing data could not be acquired due to the small size of the holes. A boroscope small enough to acquire this data was not available. However, the edge finishes of all holes on all laminates were visually examined using optical microscopy techniques at $10\times-65\times$ magnification. Although no measurements could be taken, ARL-MD verified that all hole edges appeared properly broken and no discrepancies were observed.

5. Metallography

A representative longitudinal and transverse section of the strap pack laminates from 0899 and 1548 were mounted and metallographically prepared. The specimens were mounted in Bakelite with edge retention and rough-polished with 180–600-grit silicon carbide paper. Fine-polishing was accomplished with hand-polishing wheels using 3-µm and 1-µm diamond suspensions. Final polishing was performed with a vibratory unit and 0.06-µm colloidal silica. The as-polished specimens exhibited no significant inclusions per ASTM-E-45 [11].

The polished specimens were subsequently etched with Vilella's Reagent to reveal the resultant microstructure. The longitudinal and transverse sections of this semiaustenitic stainless steel exhibited fine carbides uniformly distributed within a tempered martensitic structure as shown in Figures 9–12, respectively, for strap packs 1548 and 0899. The detrimental delta (free ferrite) phase was not apparent to any discernable degree. This structure is consistent with the prior heat treatment, cold rolling, and tempering schedule of the AM-355 precipitation hardenable stainless steel. The material conformed to the governing specification HMS 6-1073.

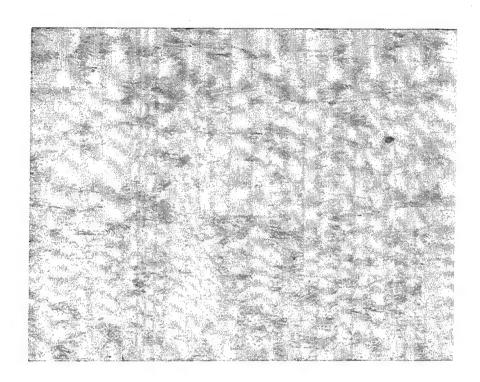


Figure 9. Micrograph of a Longitudinal Section of 1548. Vilella's Etch. Mag. $500 \times$.

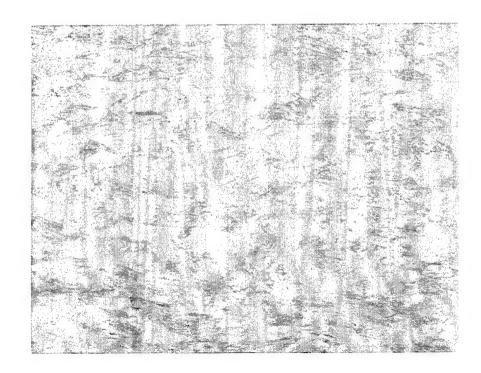


Figure 10. Micrograph of a Longitudinal Section of 0899. Vilella's Etch. Mag. 500×.

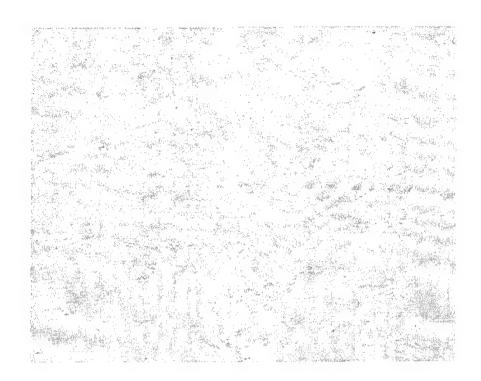


Figure 11. Micrograph of a Transverse Section of 1548. Vilella's Etch. Mag. $500 \times$.

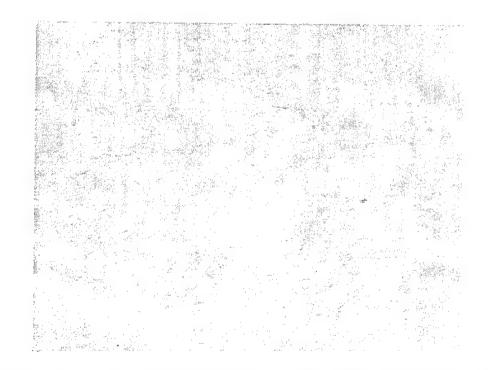


Figure 12. Micrograph of a Transverse Section of 0899. Vilella's Etch. Mag. 500x.

6. Conclusions

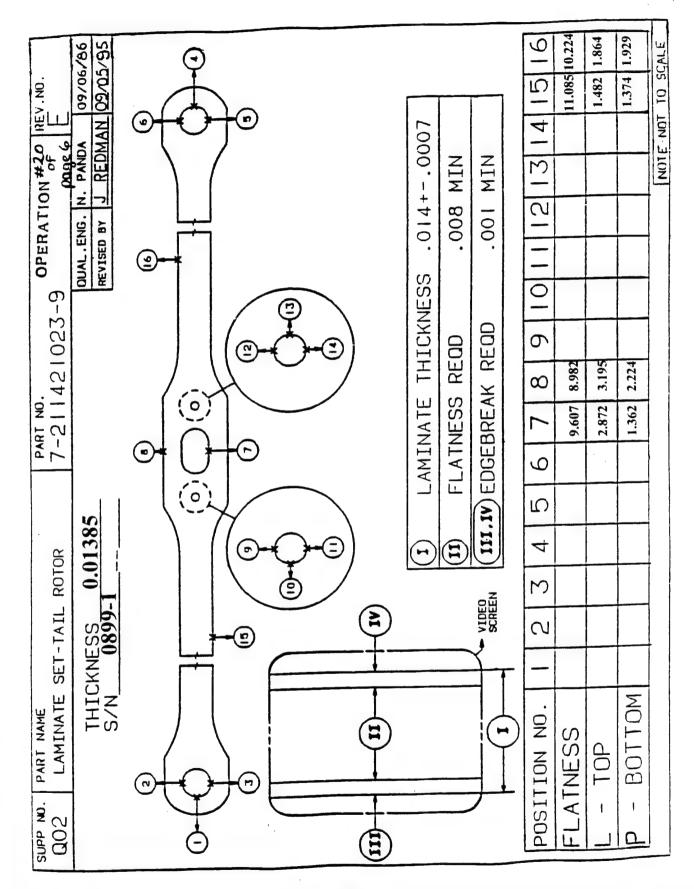
The examination revealed that, for the two assembly QDR exhibits, the buckling along the length was caused by a combination of controlling factors. The first being a dimensional nonconformity with respect to the hole diameters, and the second being a transposition about the Y-axis of the part that is not perfectly symmetric. All assembly laminates examined were found to have hole diameters smaller than allowed per the specified part drawing BP-7-211421023. The unassembled laminate sets were also examined and were found to contain the same dimensional nonconformity. The transposition of the respective positions of the laminates within the pack is prohibited after hole boring or reaming, per EPB-4-321, para. 3.3.1.3.1 [4]. However, considering the laminates may have the finishing operations performed individually or in subsets of the pack, a Y-axis transposition of a laminate with respect to its rotational orientation is most likely the root-cause of the buckling, since it is not distinctly prohibited per the specification (refer to the discussion section). All other characteristics of the laminates and assemblies were found to conform to the governing part drawings and specifications.

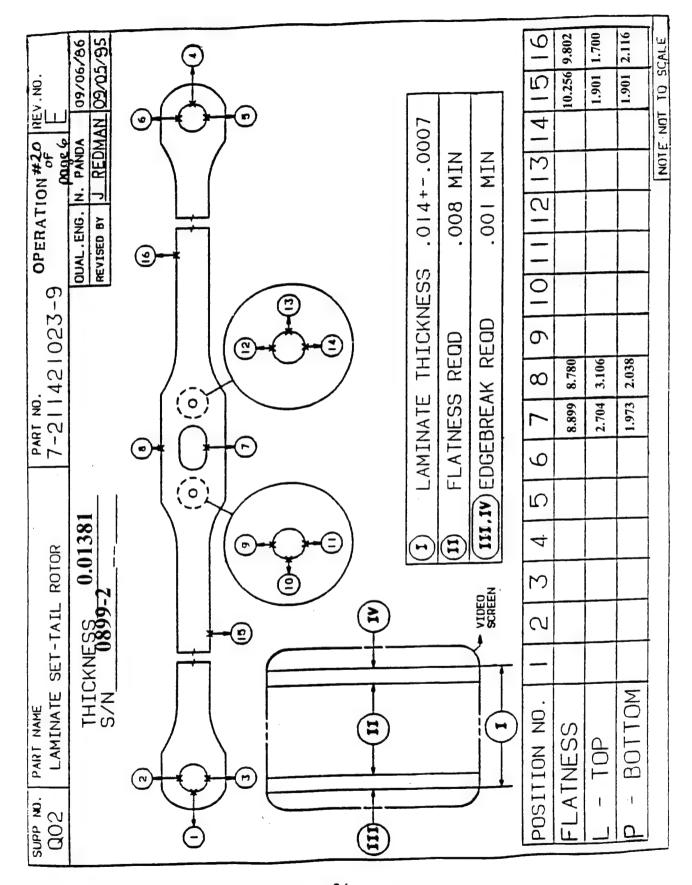
7. References

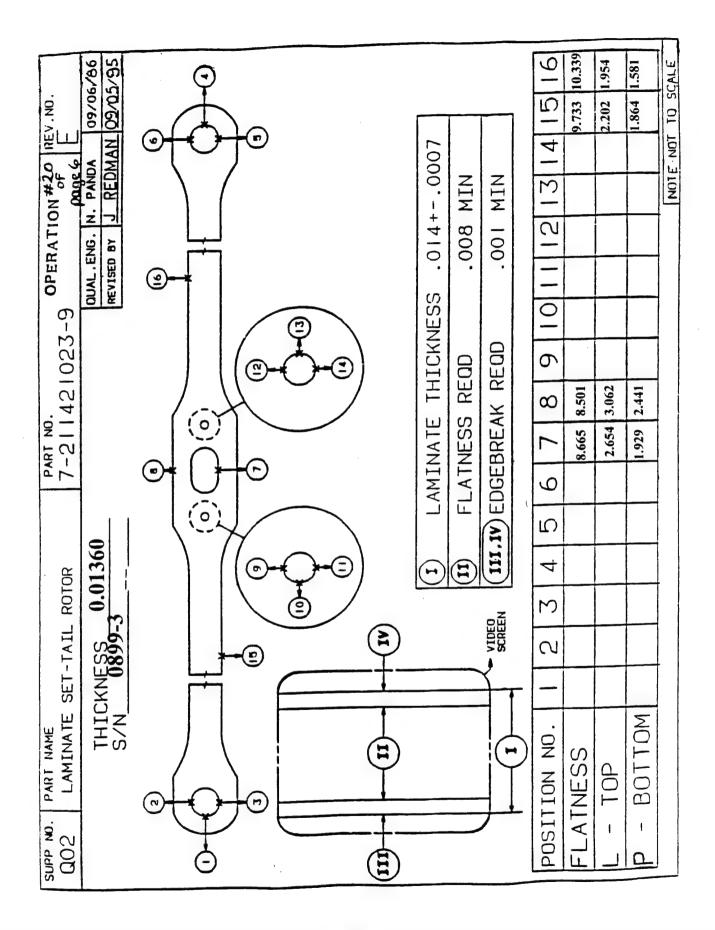
- 1. Lockheed Support Systems, Inc. "Quality Deficiency Report for Exhibit Part Number 7-211421035-5 and Serial Number 003343-0899." W81CL8940027, Fort Hood Army Airfield, Fort Hood, TX, 8 March 1994.
- 2. Lockheed Support Systems, Inc. "Quality Deficiency Report for Exhibit Part Number 7-211421035-5 and Serial Number 003343-1548." W81CL8940085, Fort Hood Army Airfield, Fort Hood, TX, 16 November 1994.
- 3. McDonnell Douglas Helicopter Company. "Strap Assembly Tail Rotor." Drawing Package BP-7-211421035, 5000 East McDowell Road Mesa, AZ, 4 April 1991.
- 4. McDonnell Douglas Helicopter Company. "Finishing Holes, Edges, and Surfaces of AH-64 Main and Tail Rotor Blade Retention Laminates." Engineering Process Bulletin 4-321 (EPB-4-321), Revision E, 5000 East McDowell Road, Mesa, AZ, 3 June 1994.
- 5. McDonnell Douglas Helicopter Company. "Strap Assembly Tail Rotor." Drawing Package BP-7-211421035, 5000 East McDowell Road Mesa, AZ, 4 April 1991.
- 6. McDonnell Douglas Helicopter Company. "Steel, Sheet and Strip, Corrosion Resistant, AM-355 CRT (Cold Rolled and Tempered)." Material Specification HMS-6-1073 Rev. E., 5000 East McDowell Road, Mesa, AZ, 9 January 1990.
- 7. McDonnell Douglas Helicopter Company. "Identification of Detail Parts and Assemblies." Process Specification HP 8-5 Rev. T, 5000 East McDowell Road, Mesa, AZ, 8 September 1993.
- 8. McDonnell Douglas Helicopter Company. "Serialization of Parts and Subassemblies, and Numbering for Material Control." Process Specification HP 8-8 Rev. E, 5000 East McDowell Road, Mesa, AZ, 29 November 1993.
- 9. McDonnell Douglas Helicopter Company. "Bushing, Tension-Torsion Strap, Tail Rotor." Drawing Package BP-7-211421028, 5000 East McDowell Road, Mesa, AZ, 2 October 1989.
- National Aerospace Standards Committee, Aerospace Industry Association of America Inc. "Rivet-Flat Head, Hi-Shear, Close Tolerance Shank." National Aerospace Standard NAS-529, 1725 De Sales Street., NW, Washington, DC, 15 February 1983.
- 11. American Society for Testing and Materials, Standard Test Method ASTM-E-45. "Determining the Inclusion Content of Steel." 100 Barr Harbor Drive, West Conshohocken, PA, 1995.

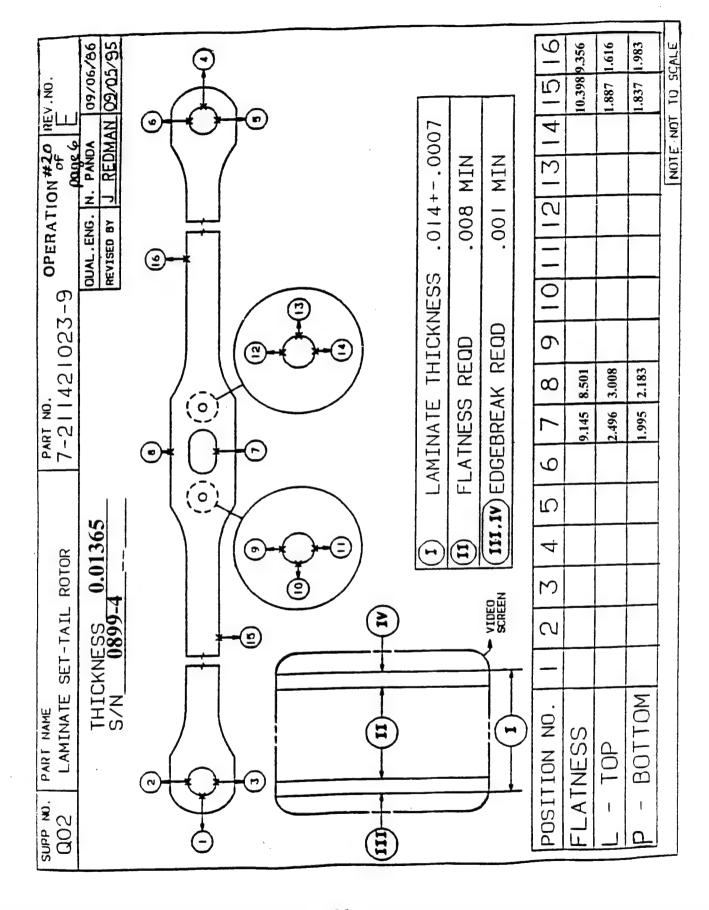
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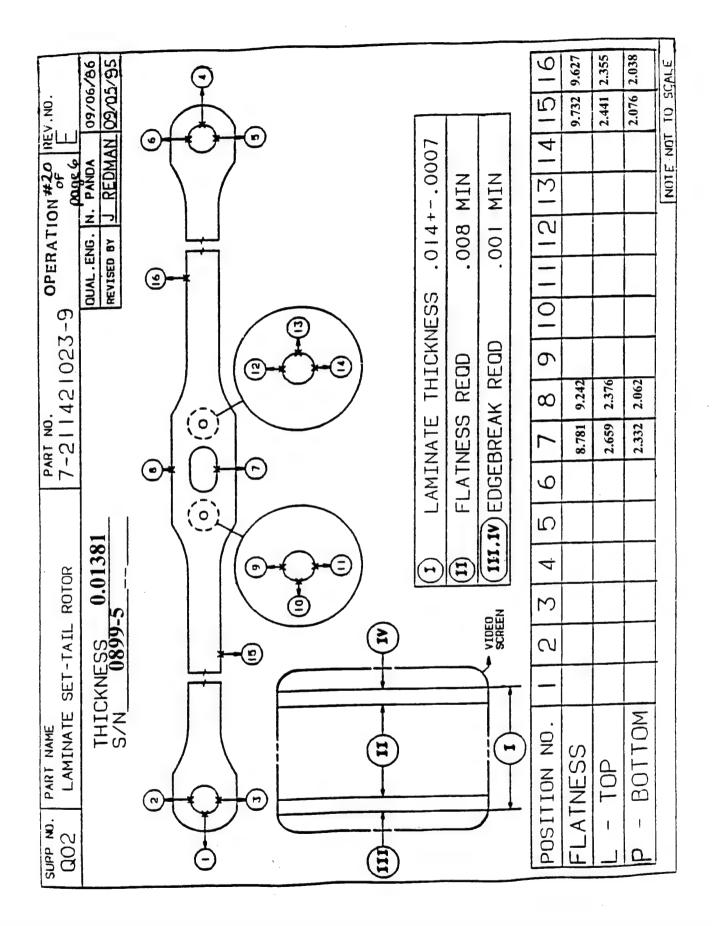
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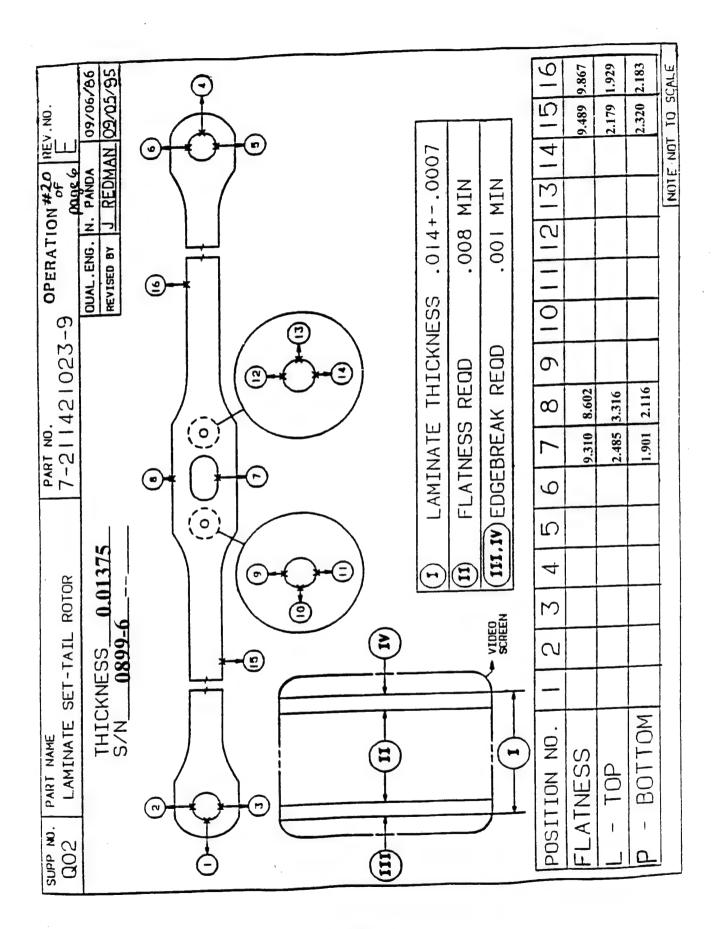


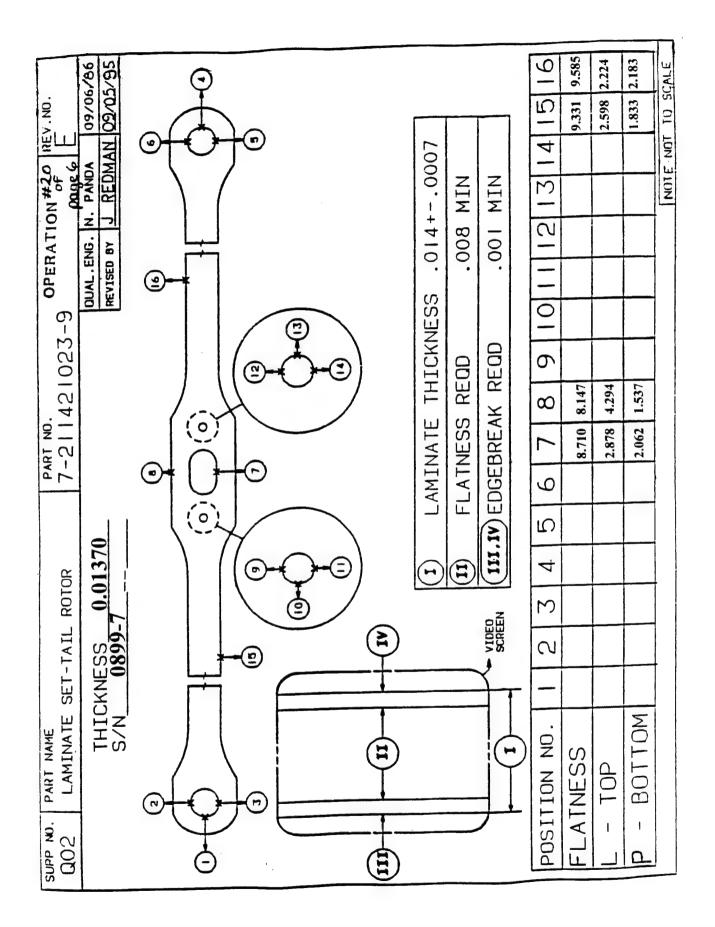


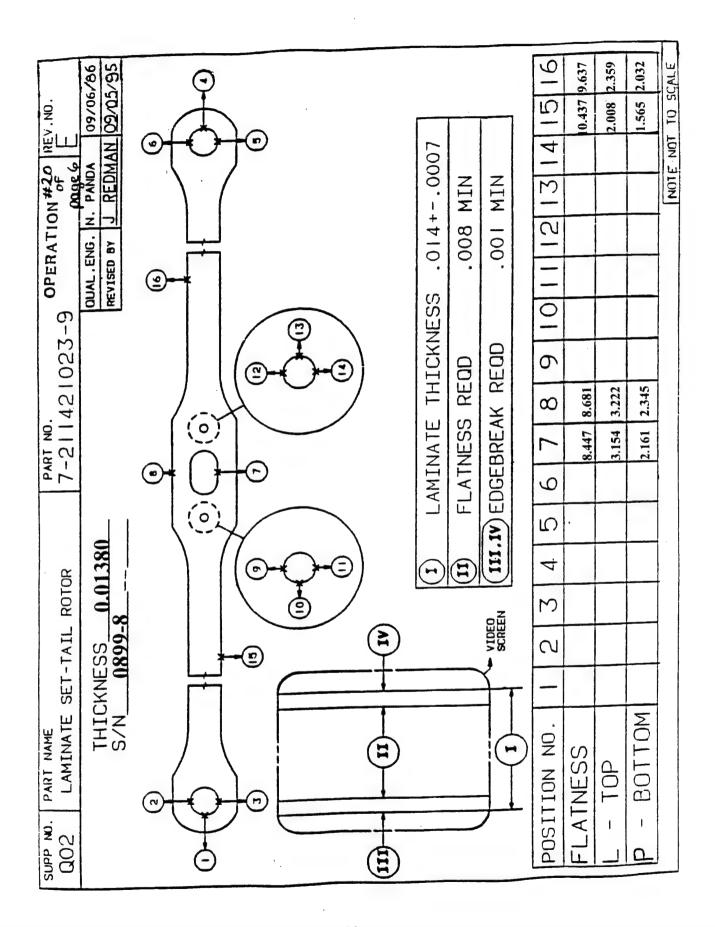


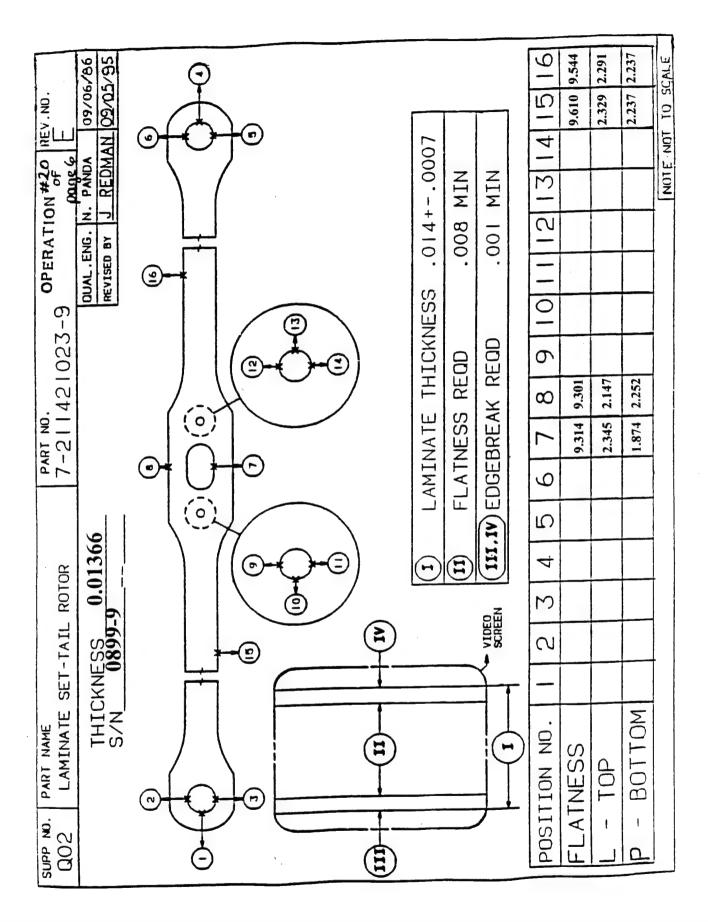


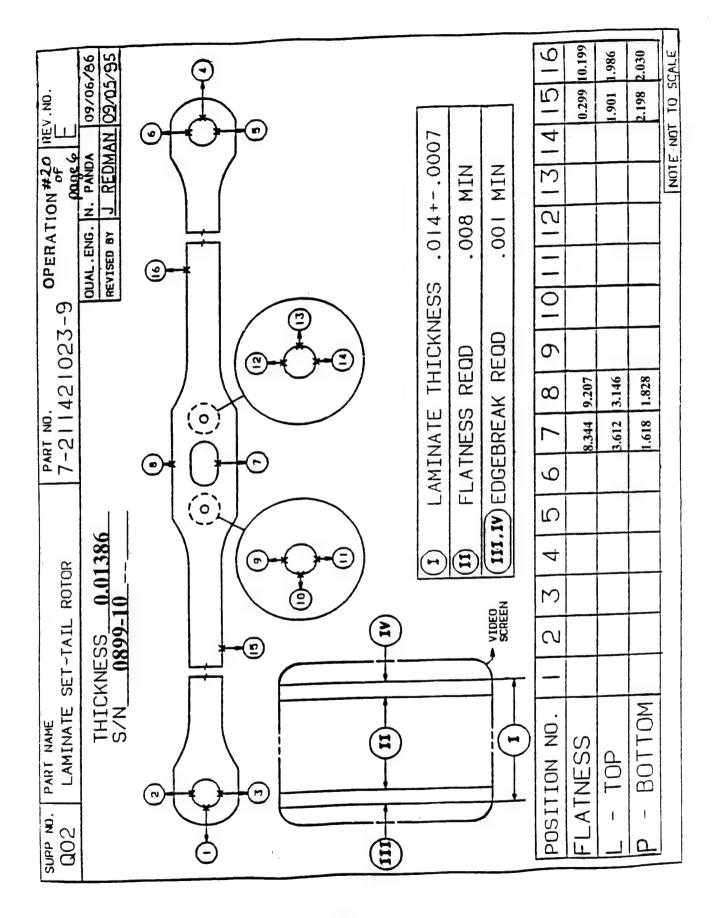


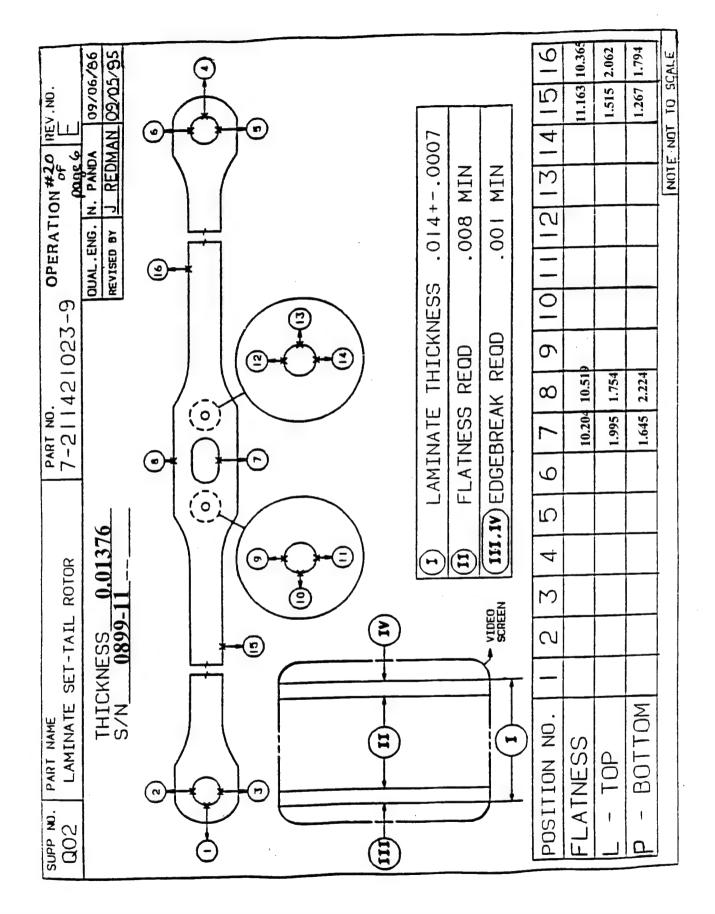


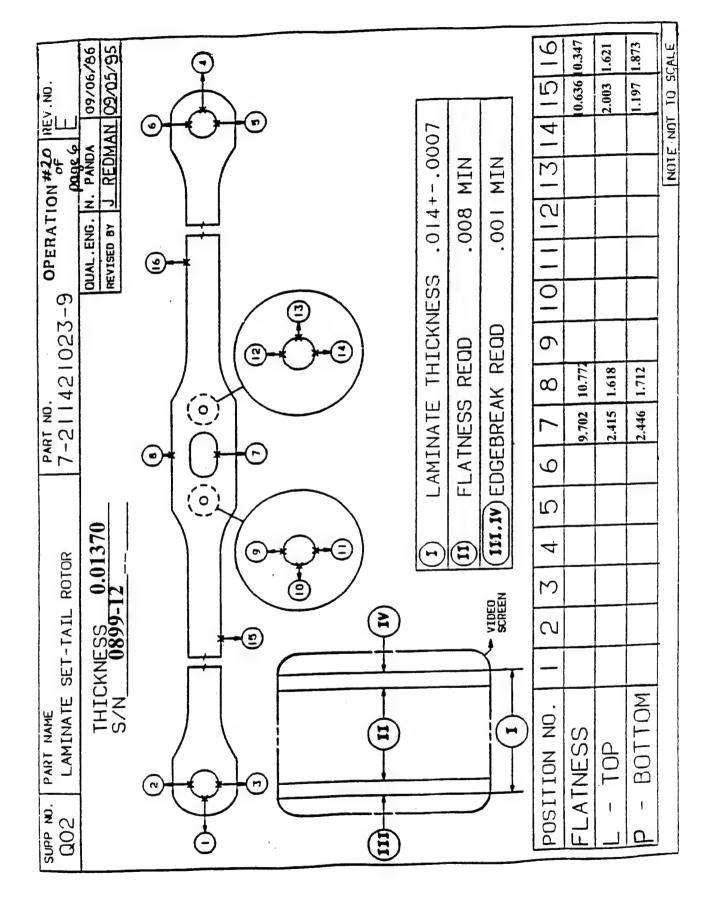


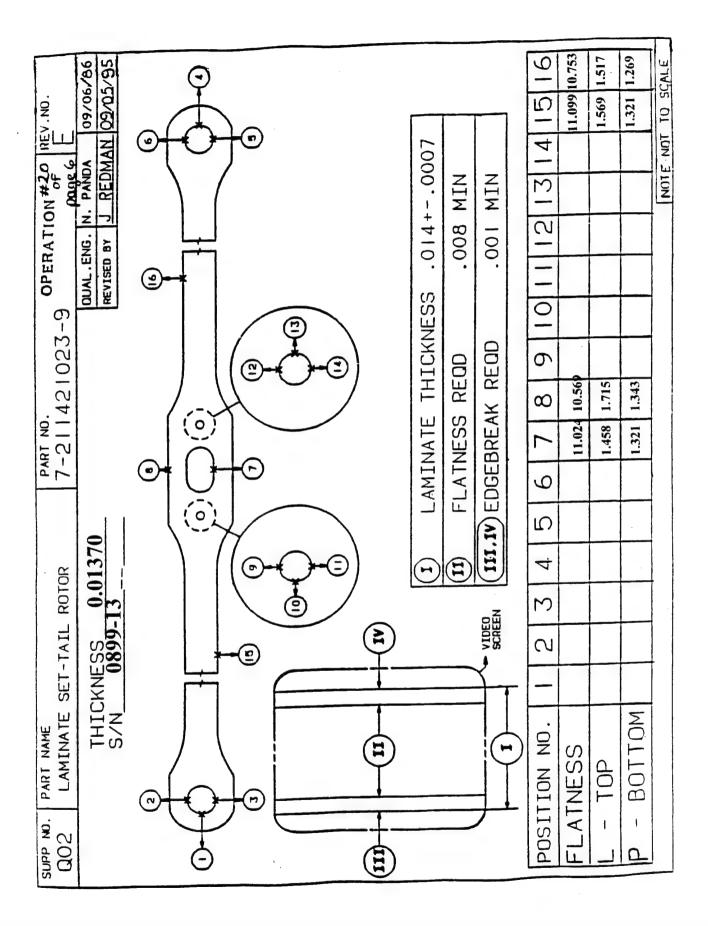


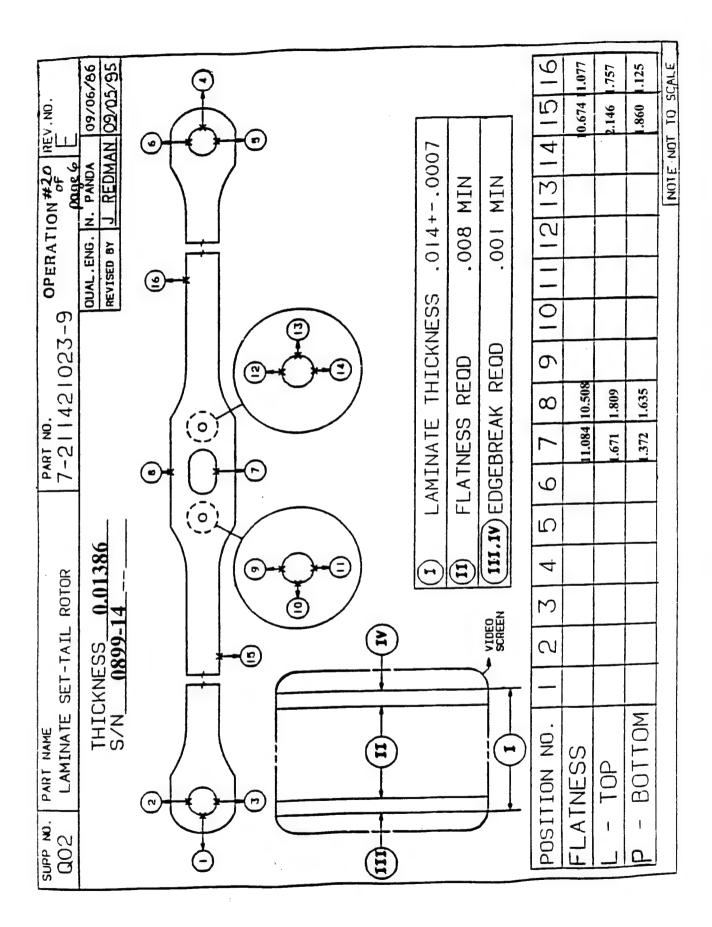


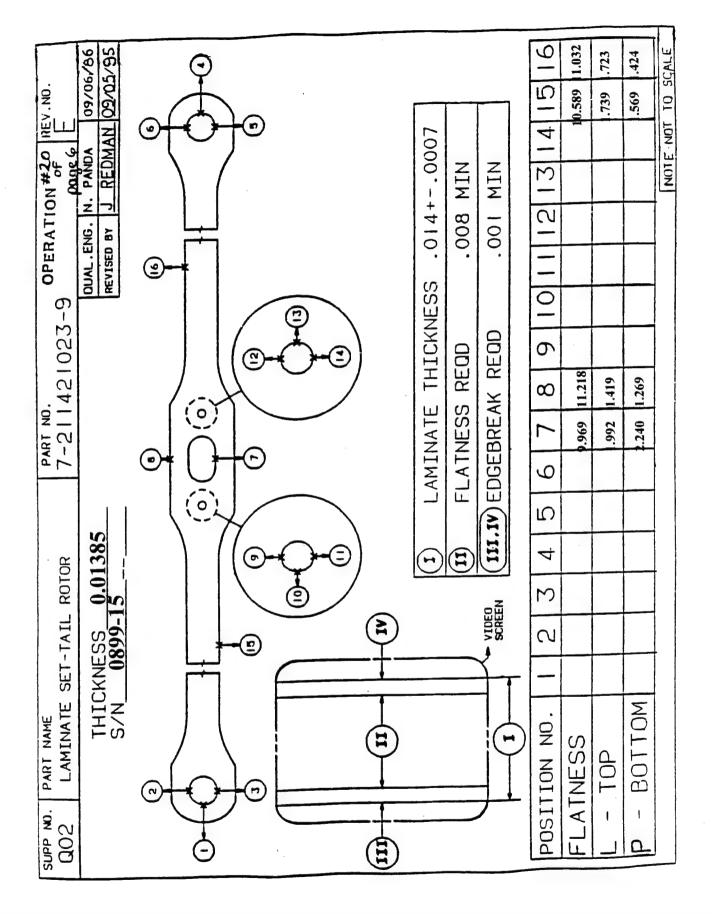


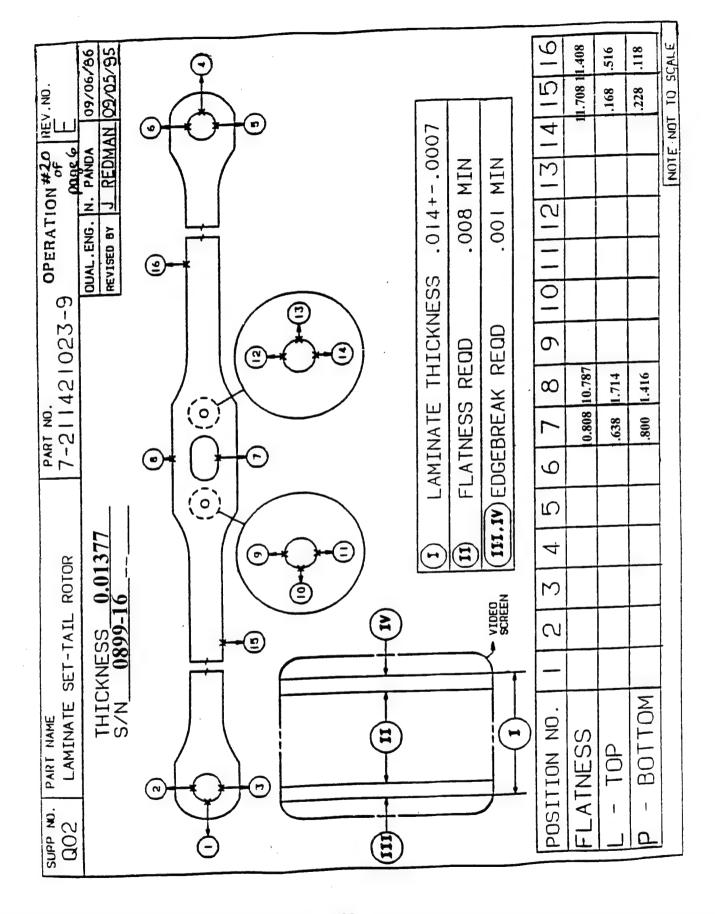


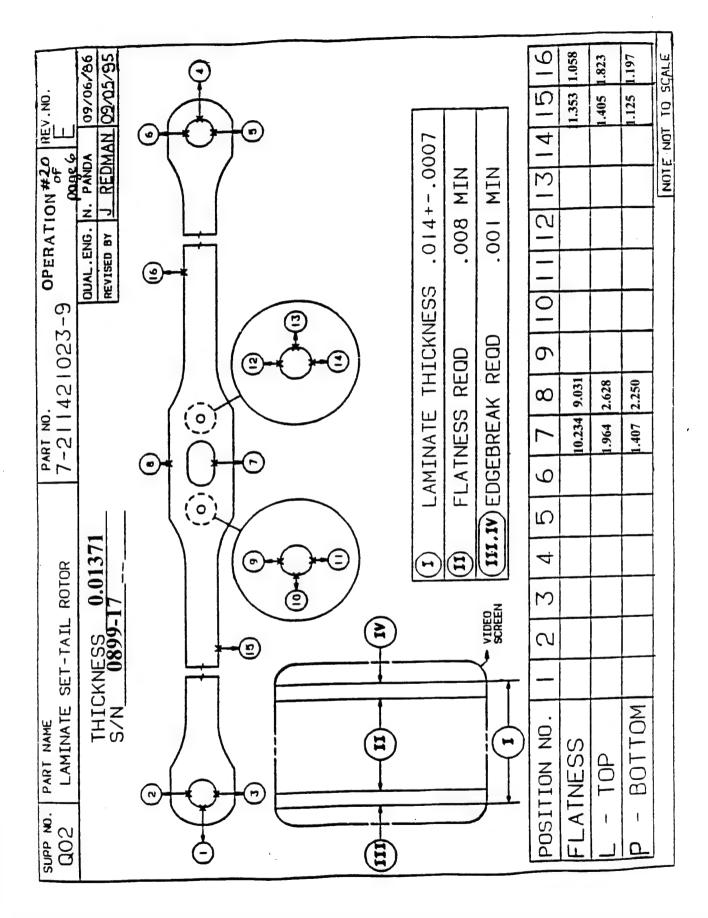


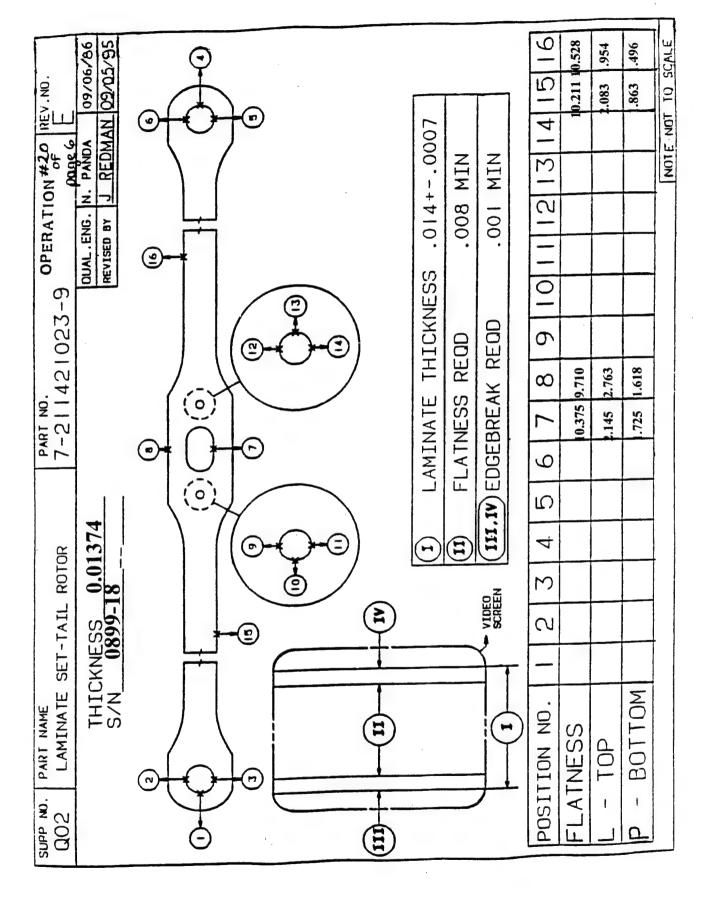


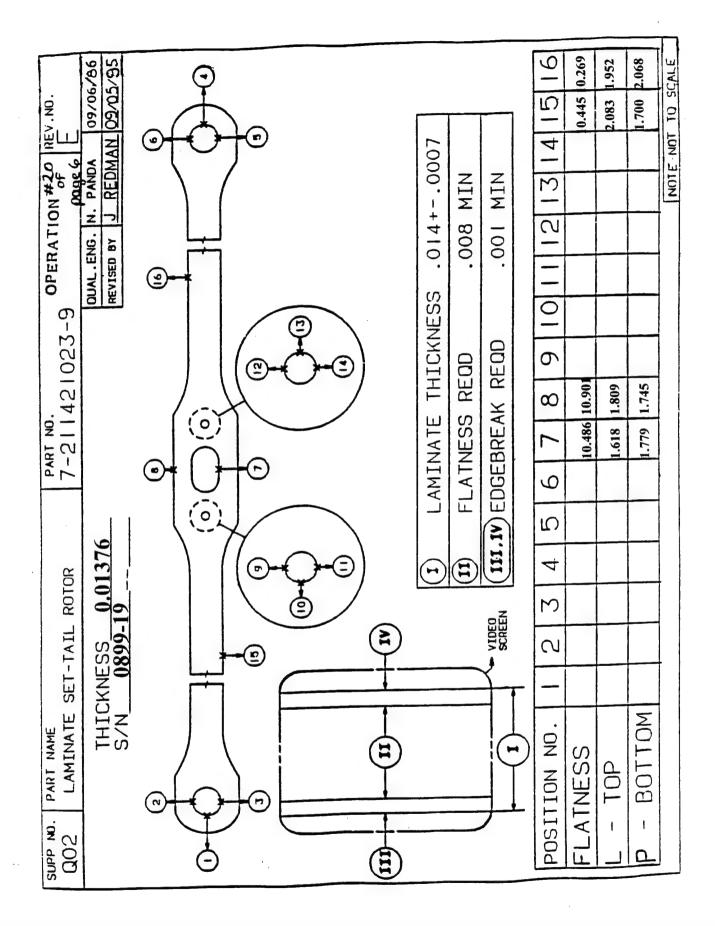


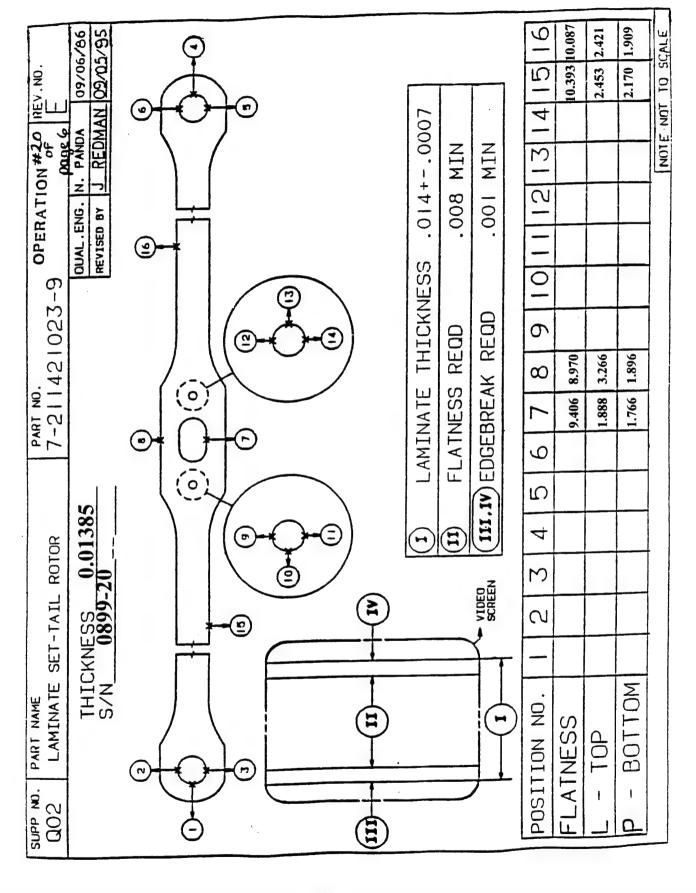


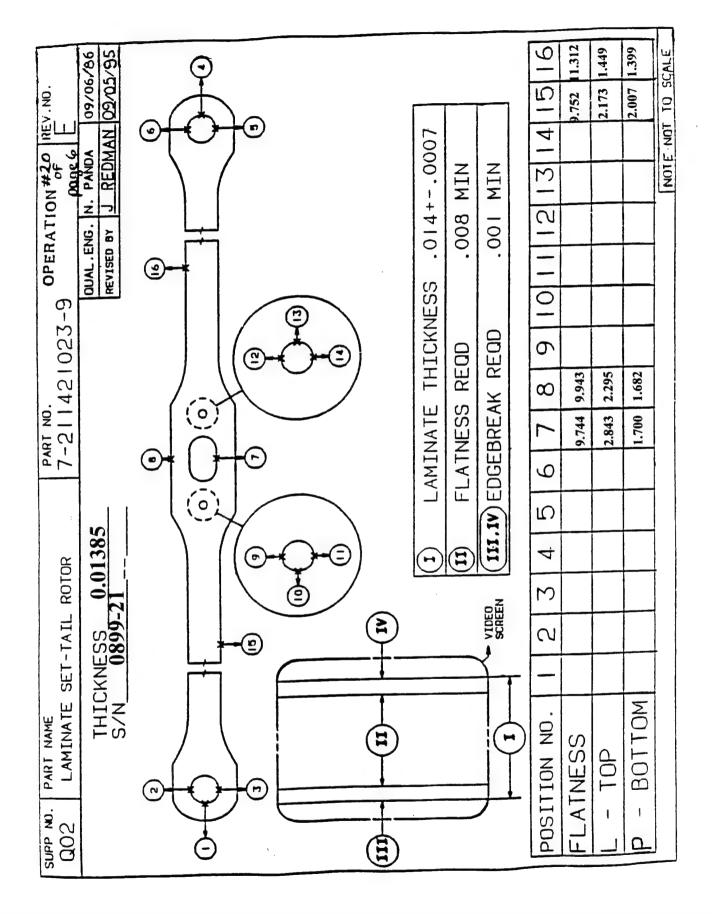


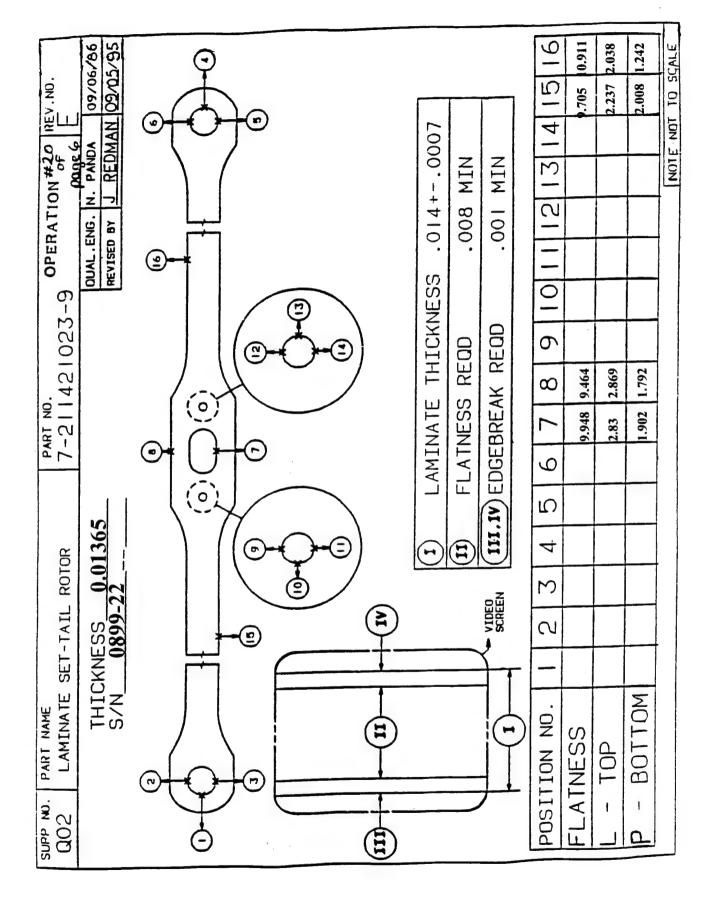








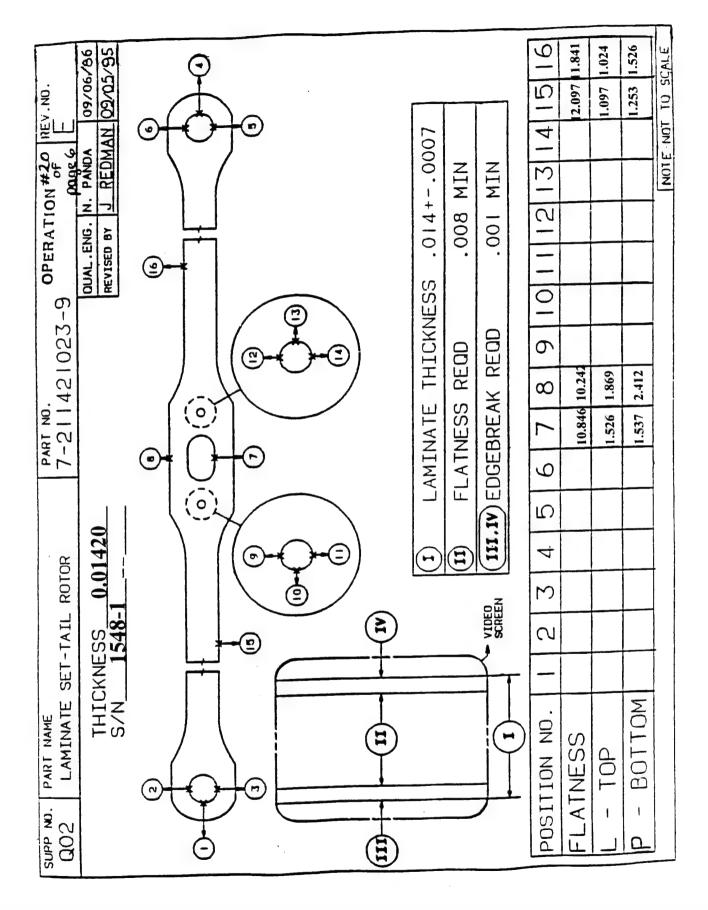


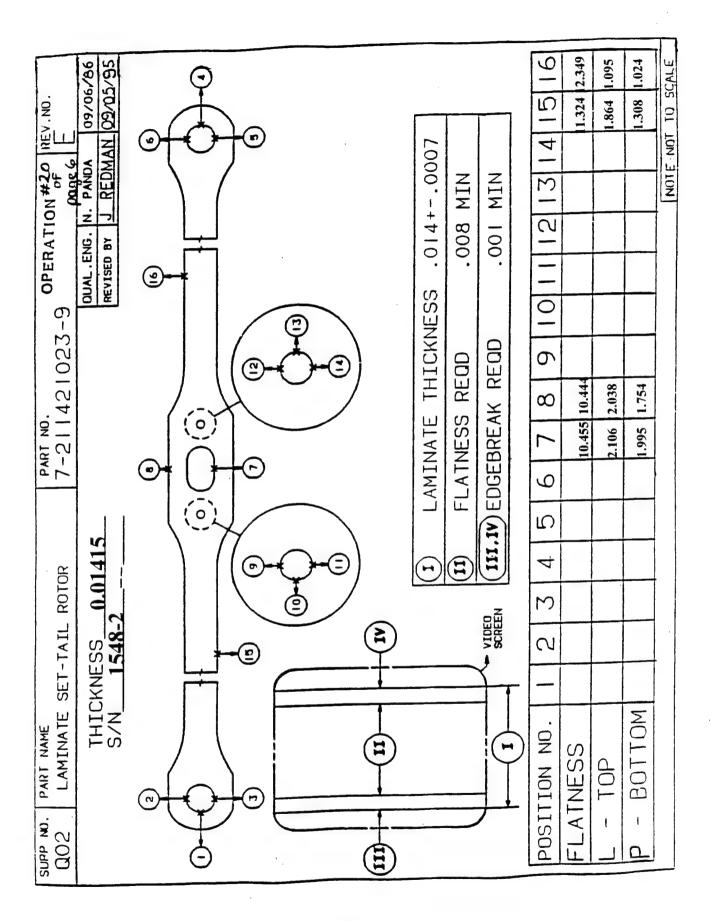


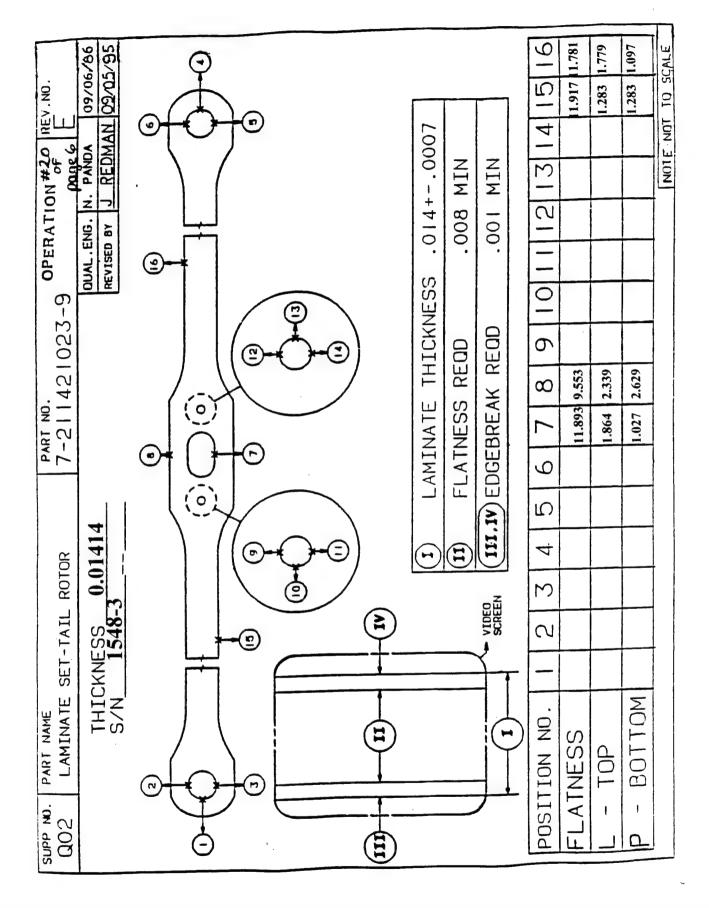
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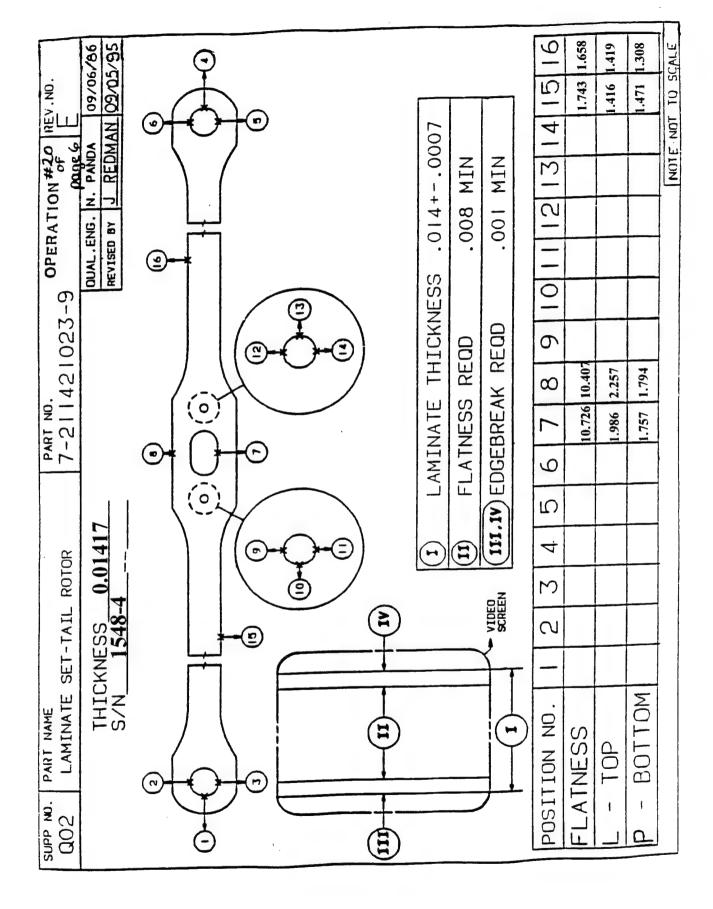
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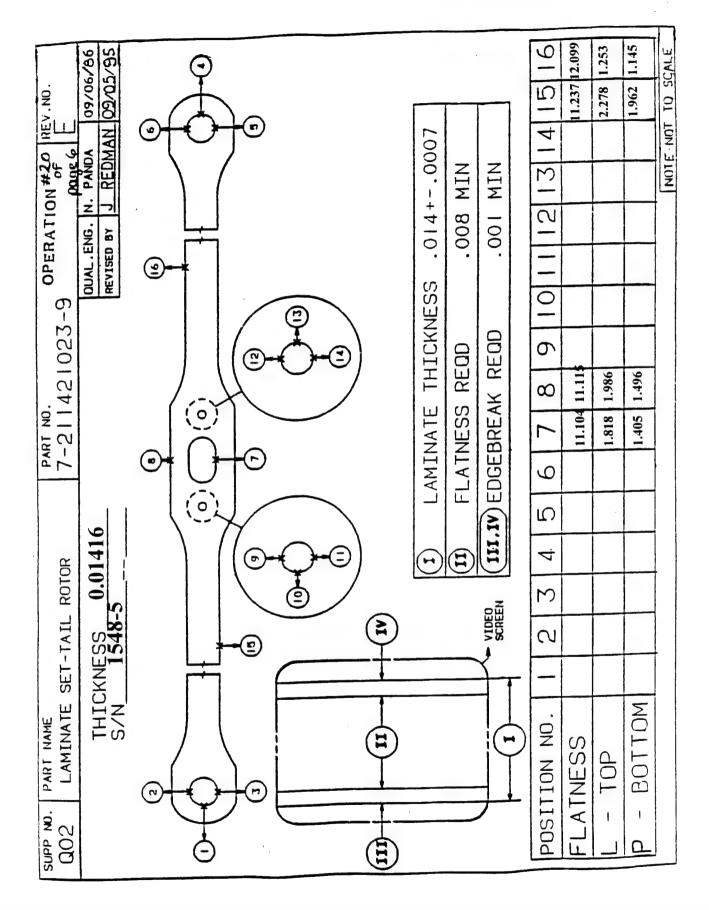
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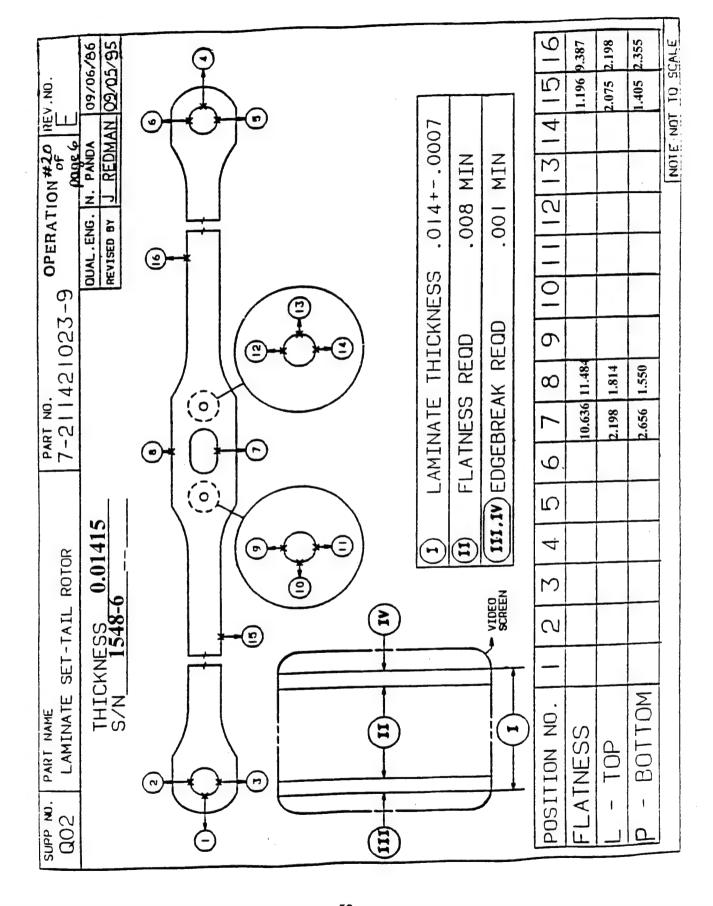


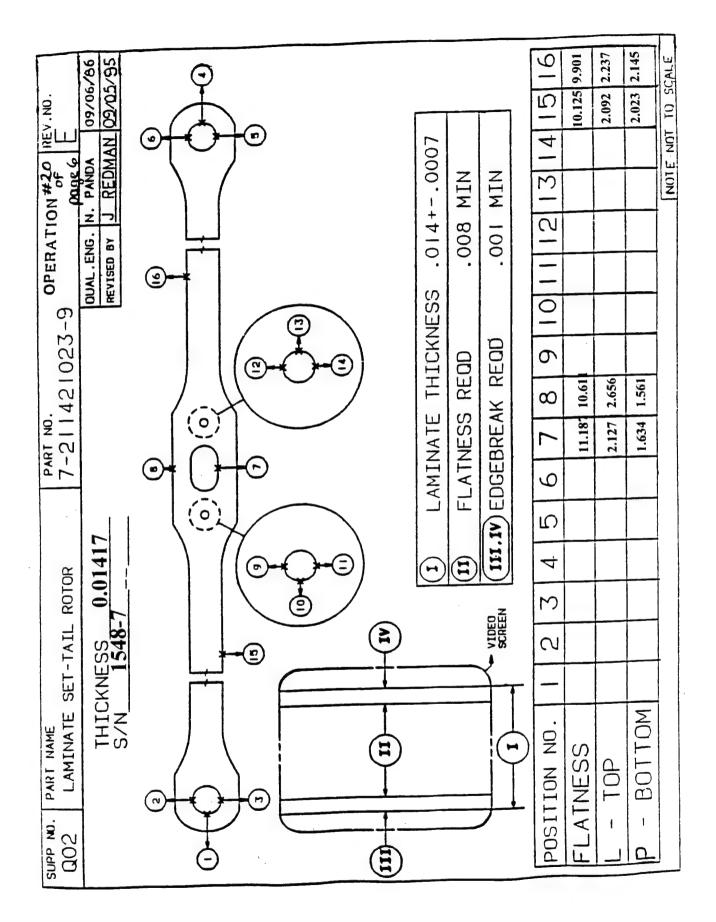


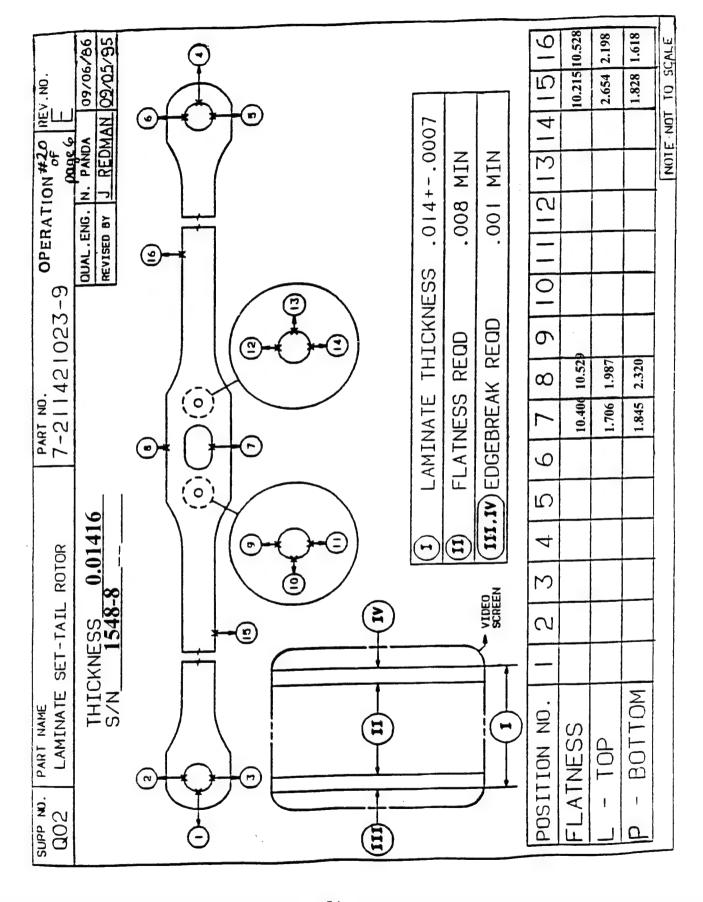


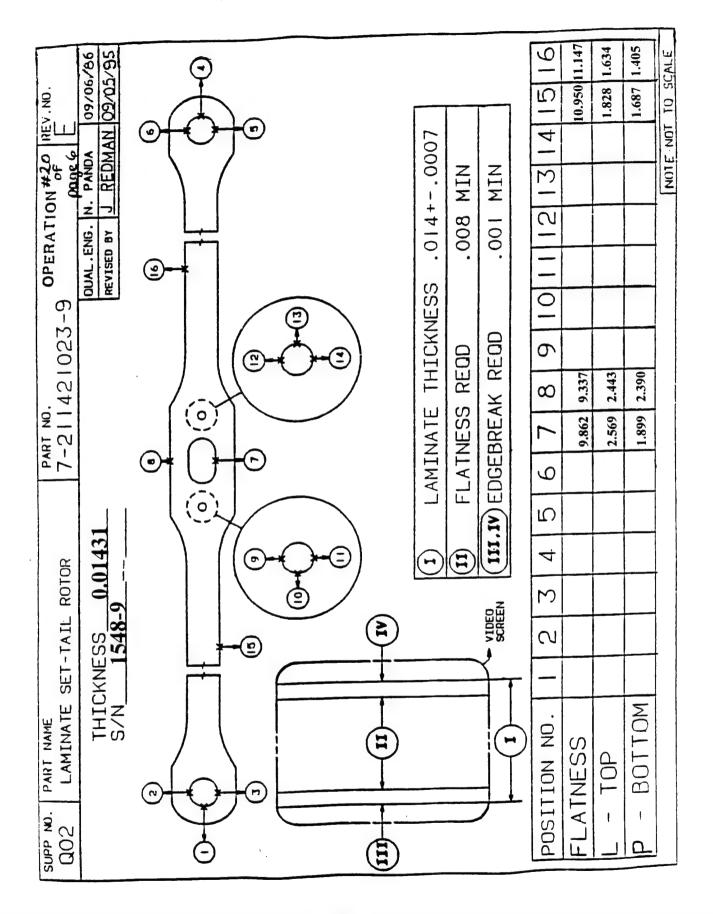


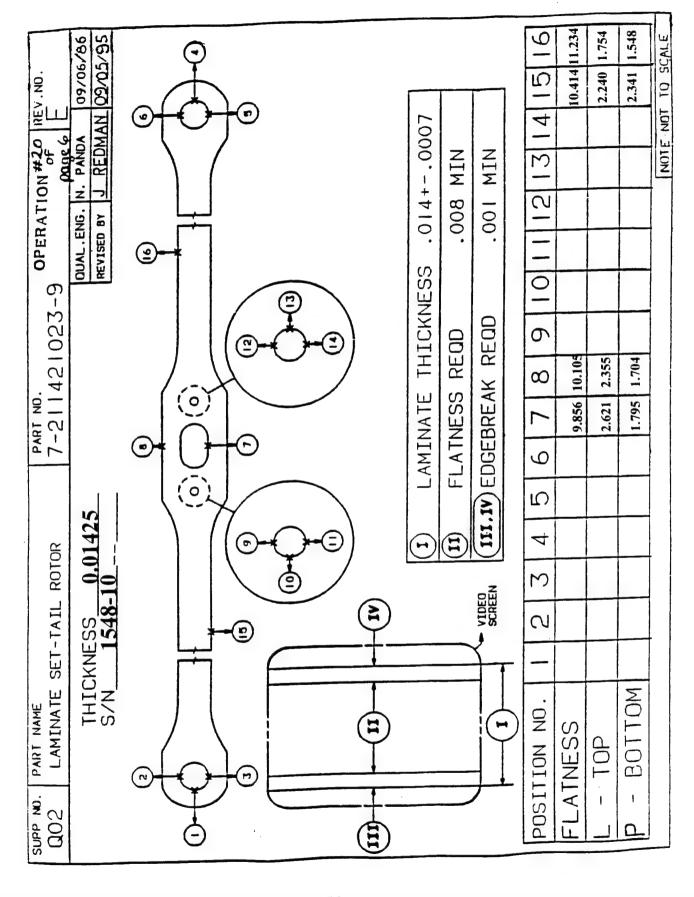


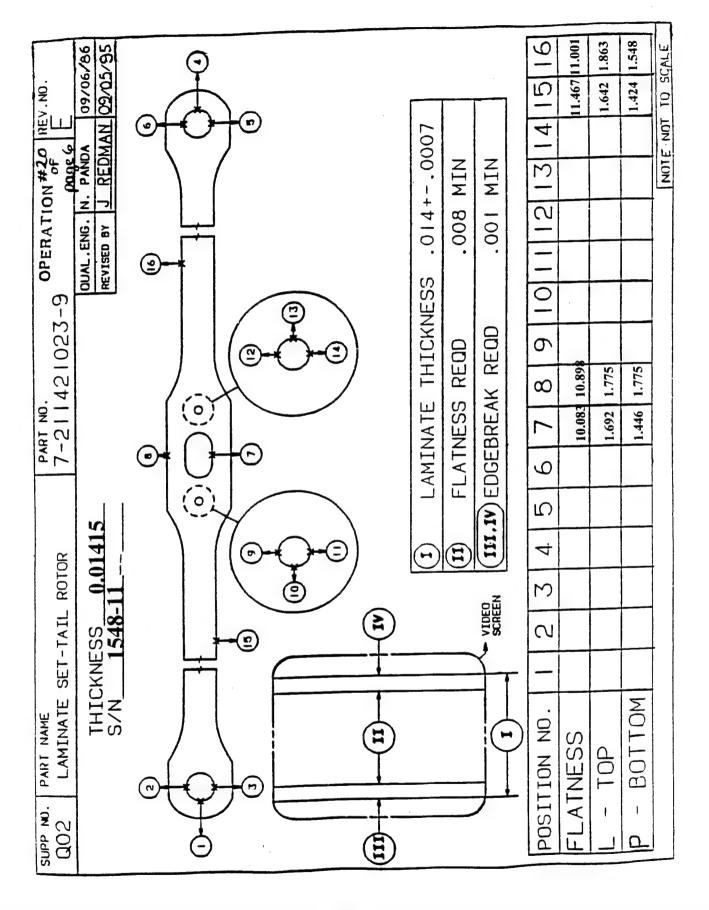


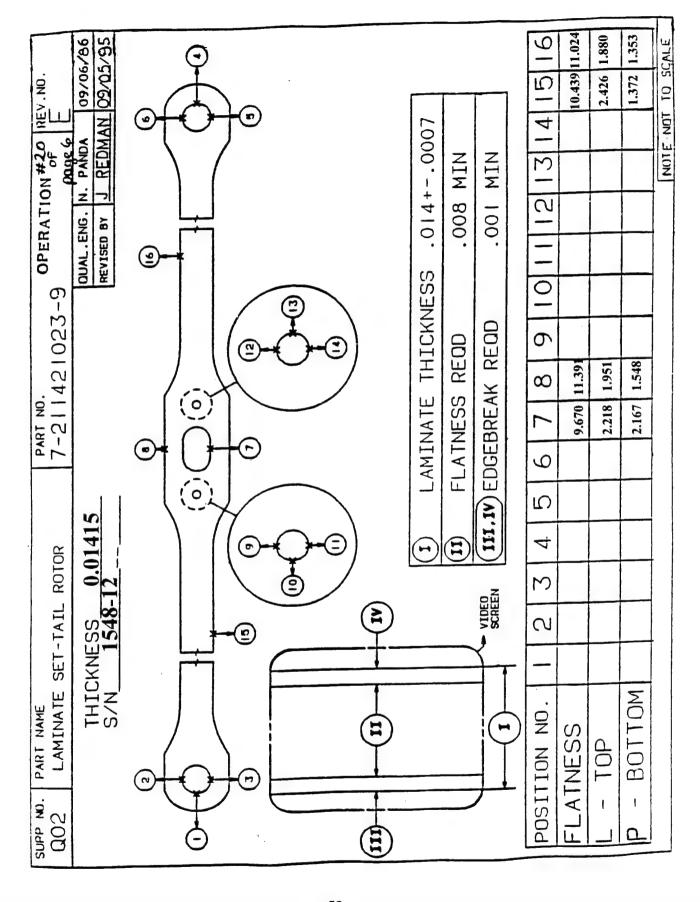


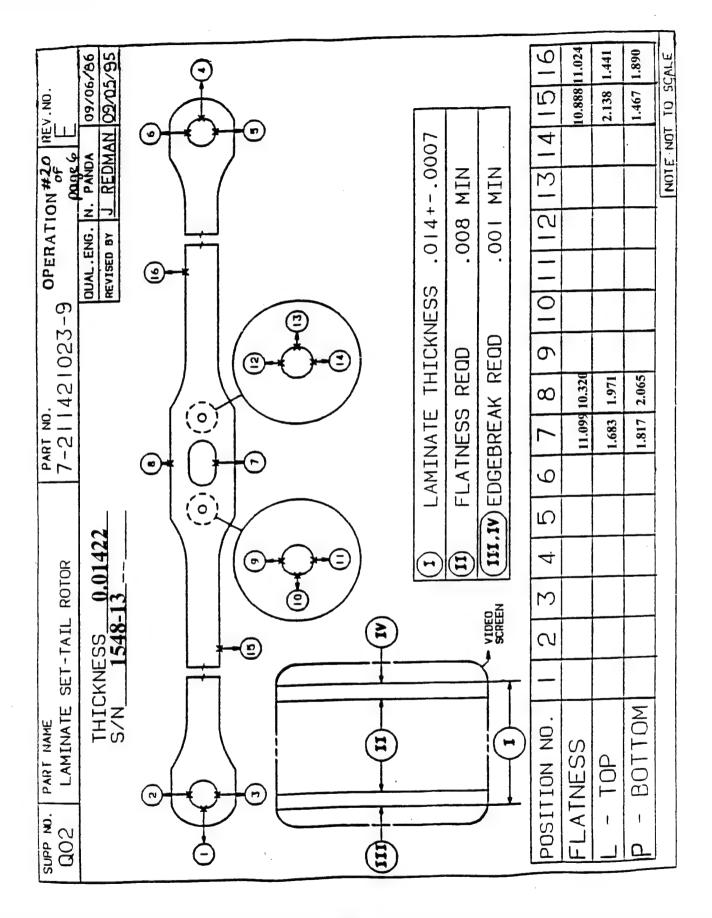


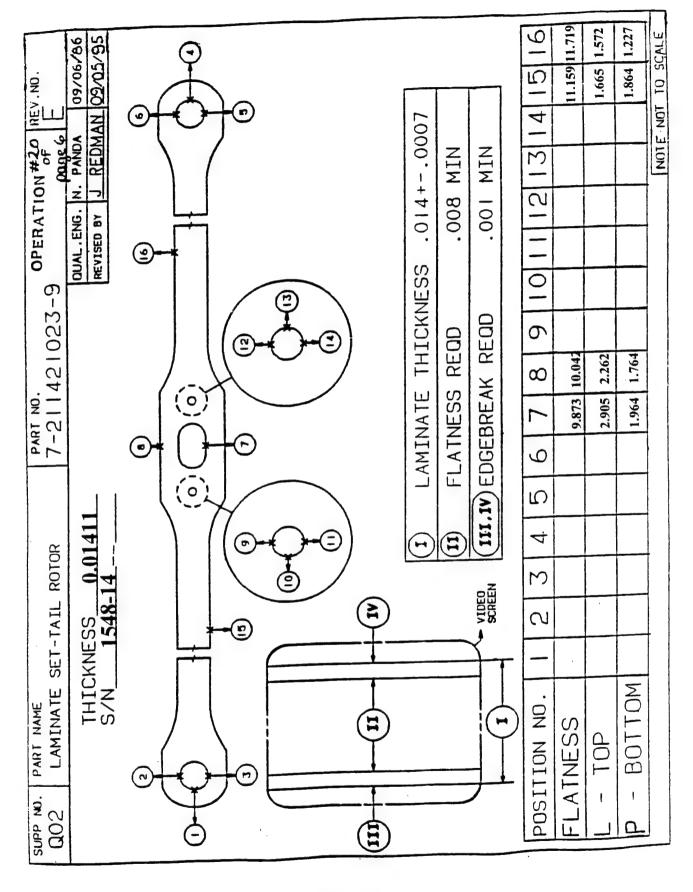


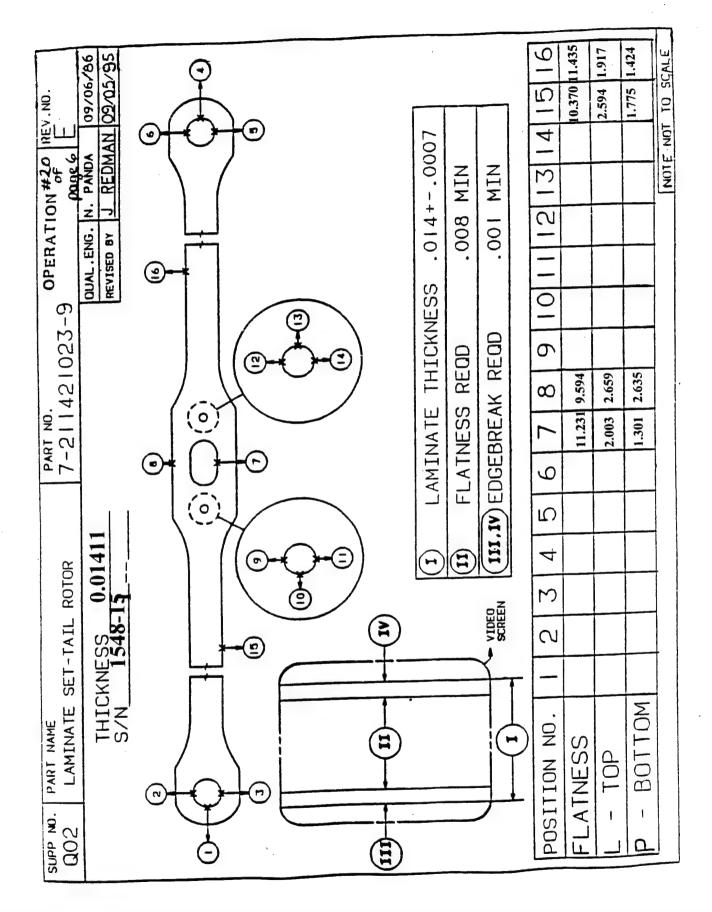


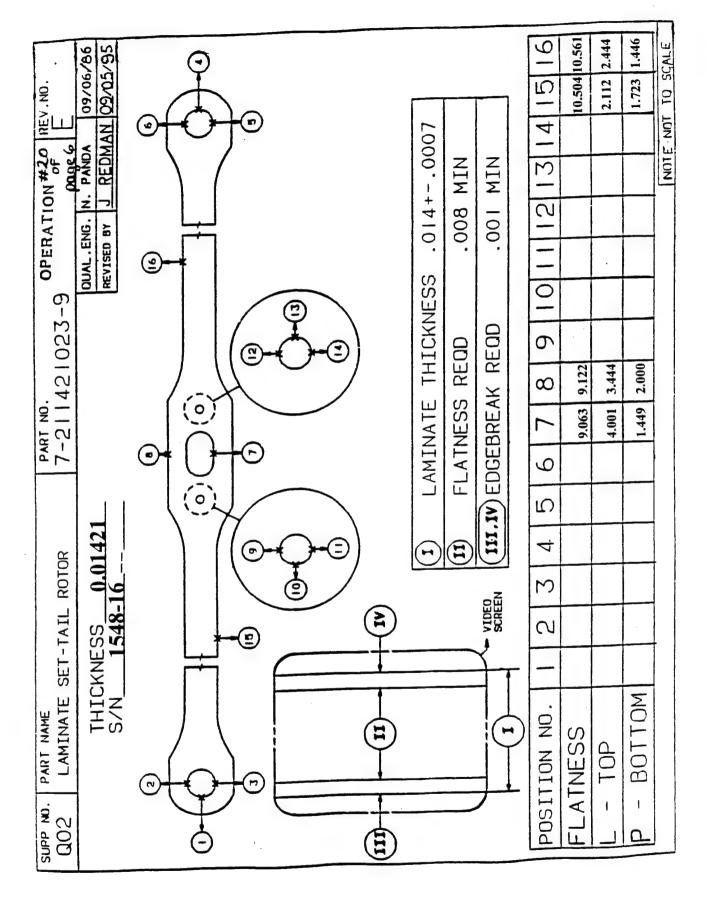


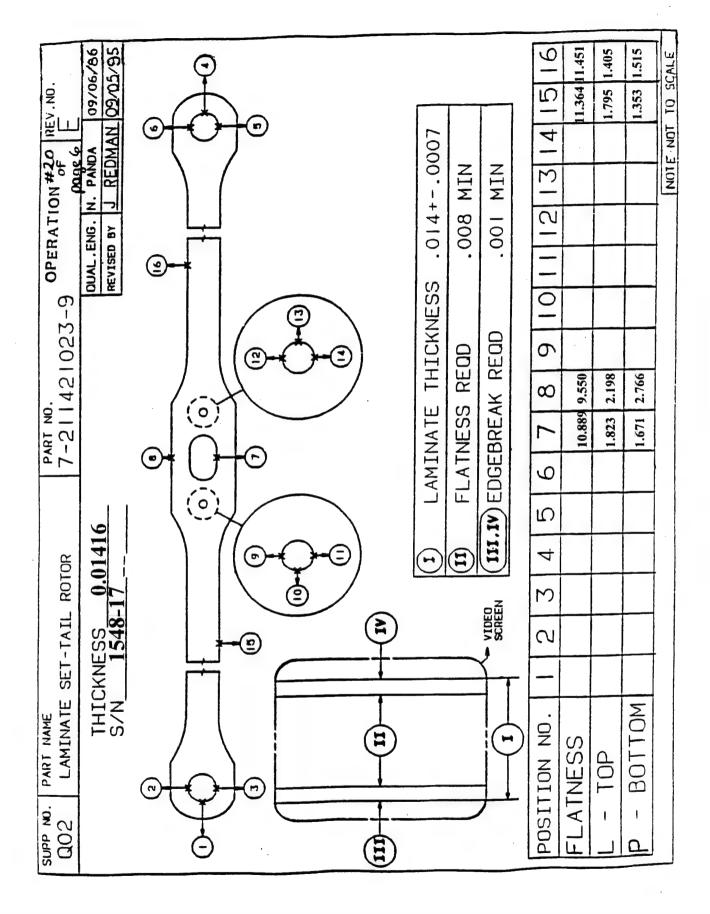


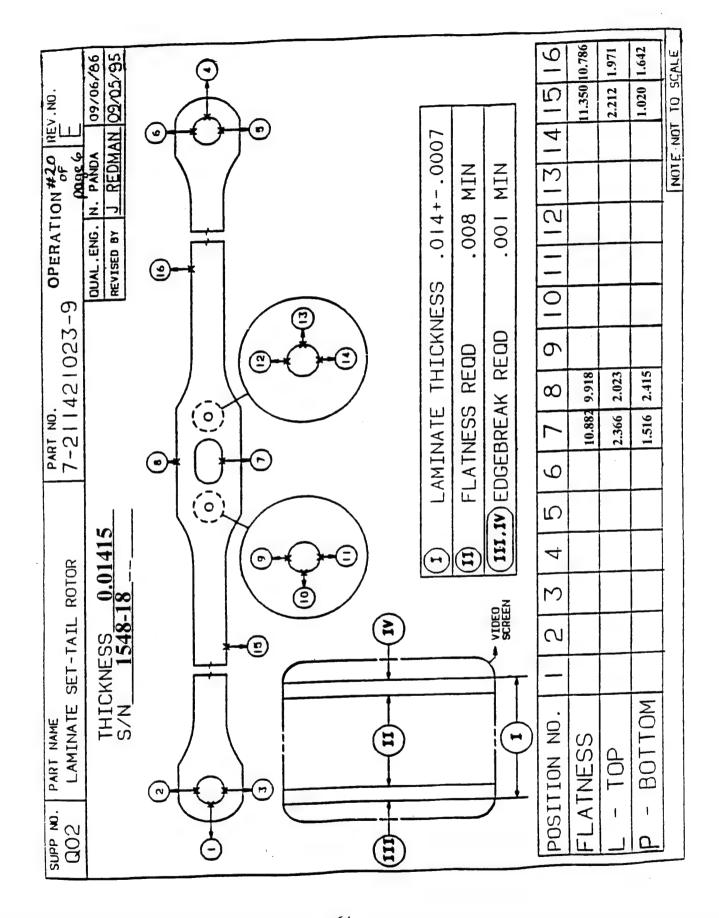


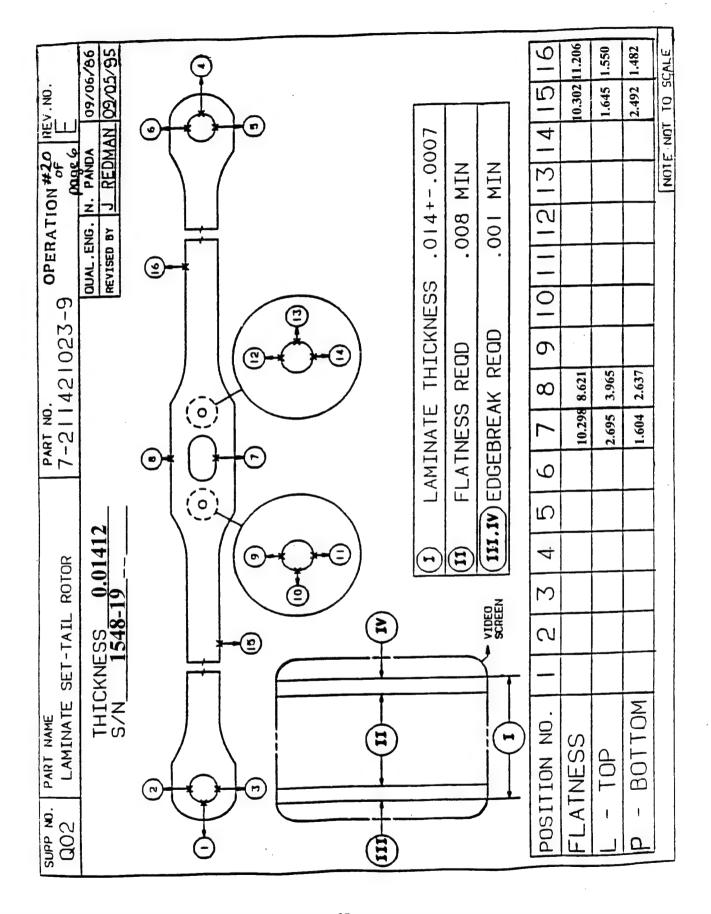


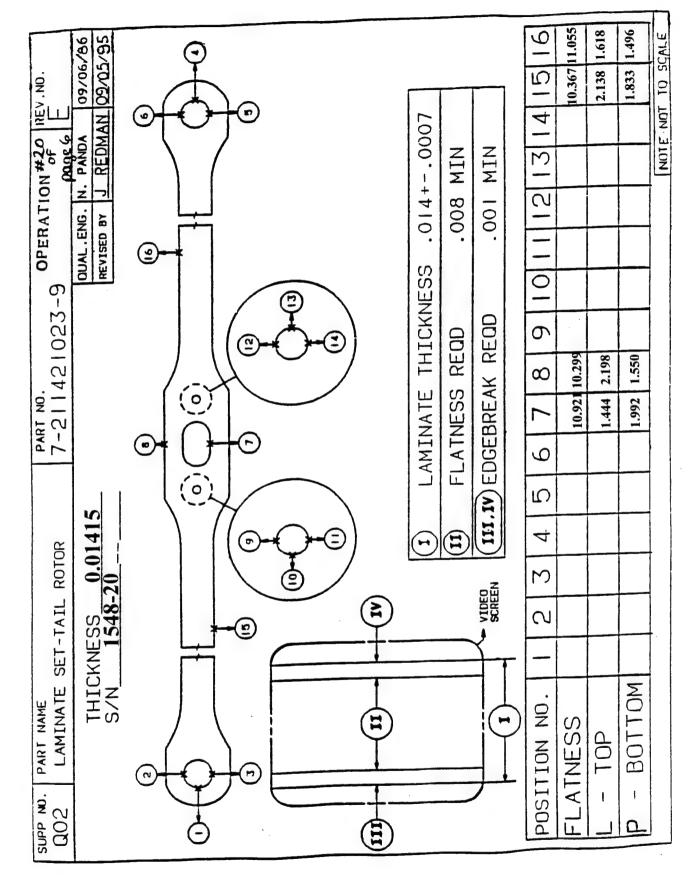


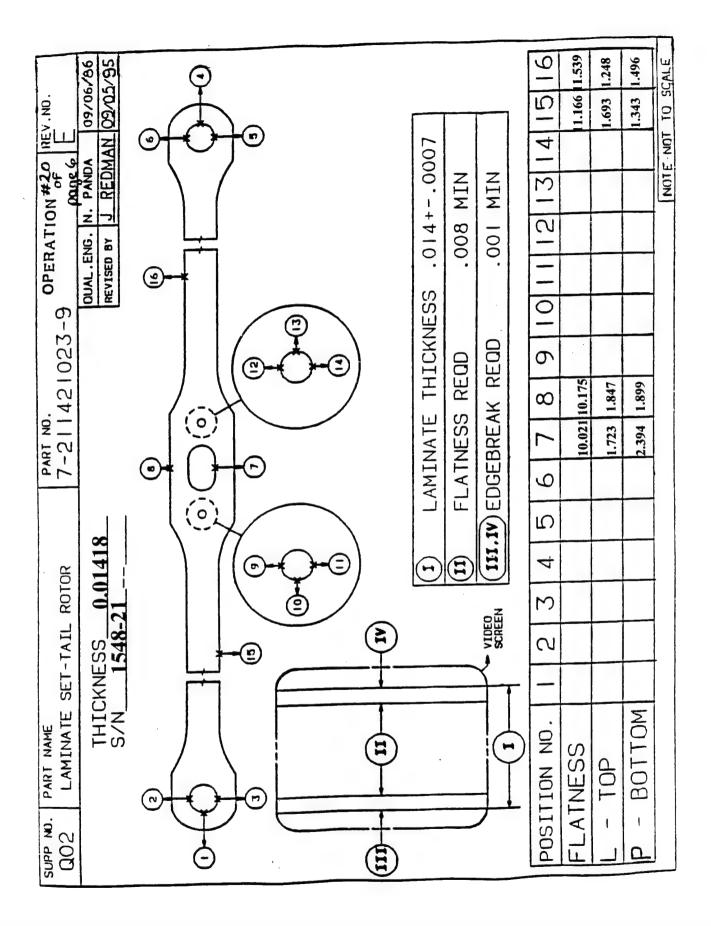


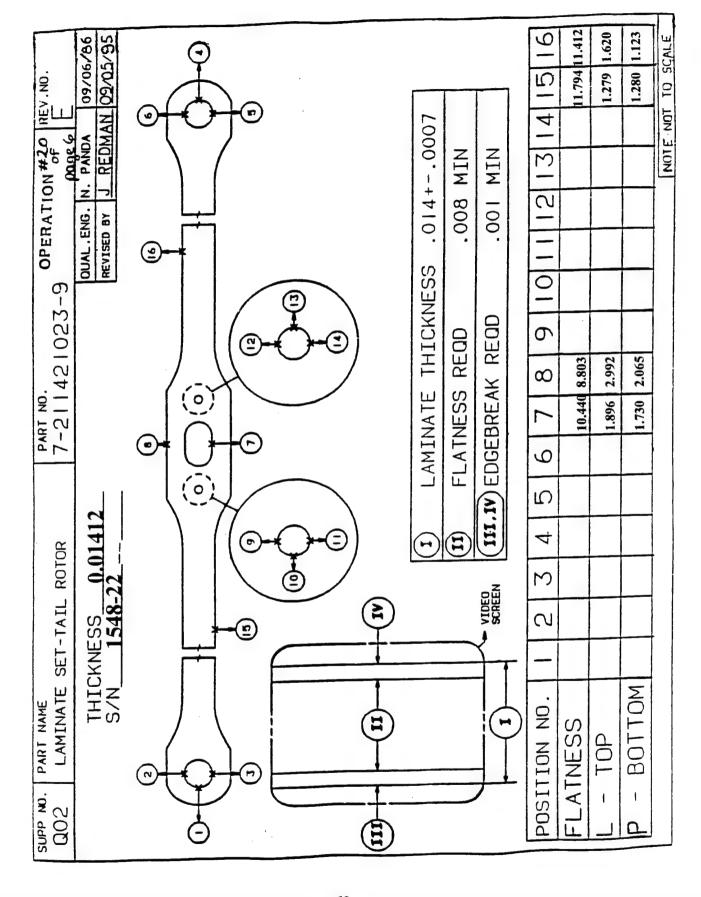








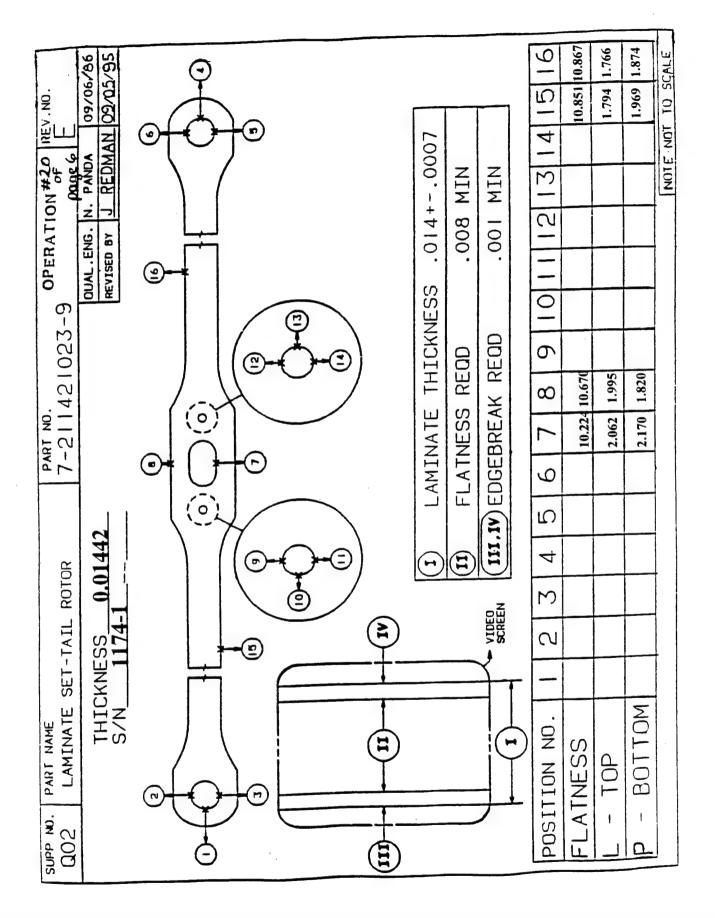


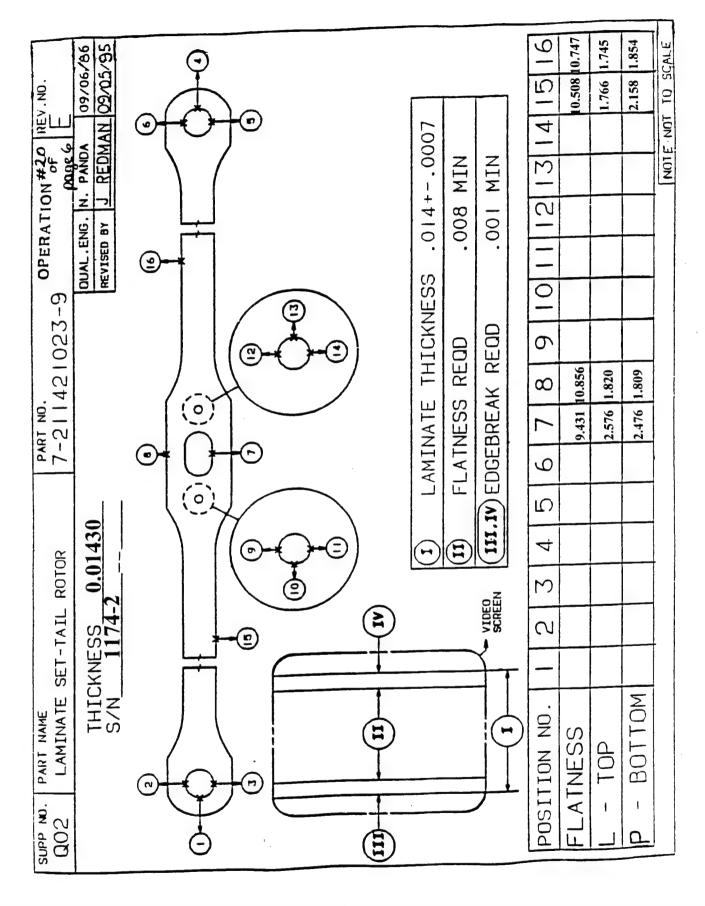


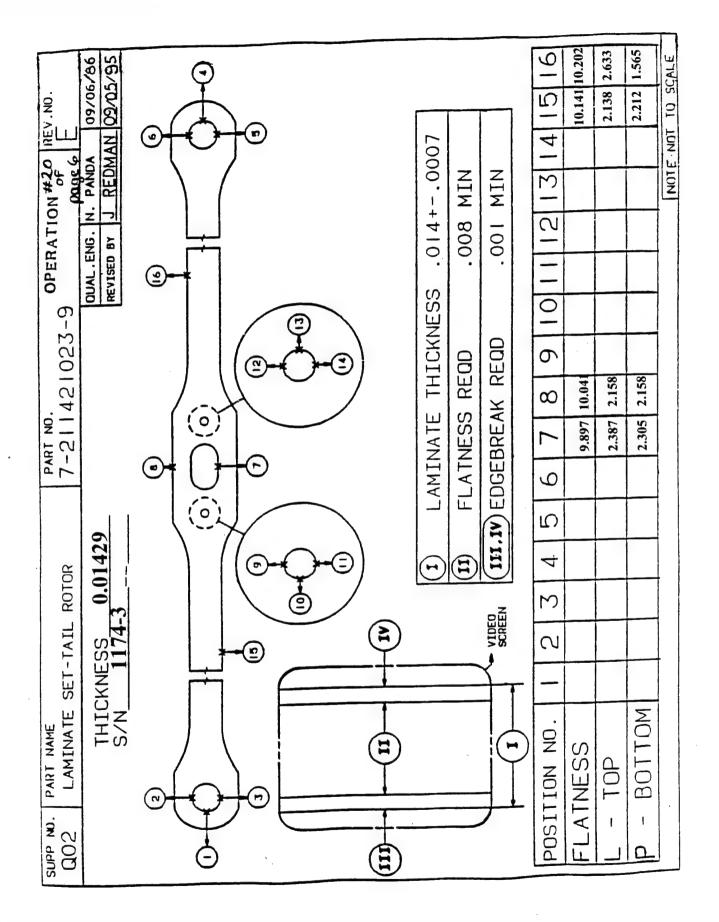
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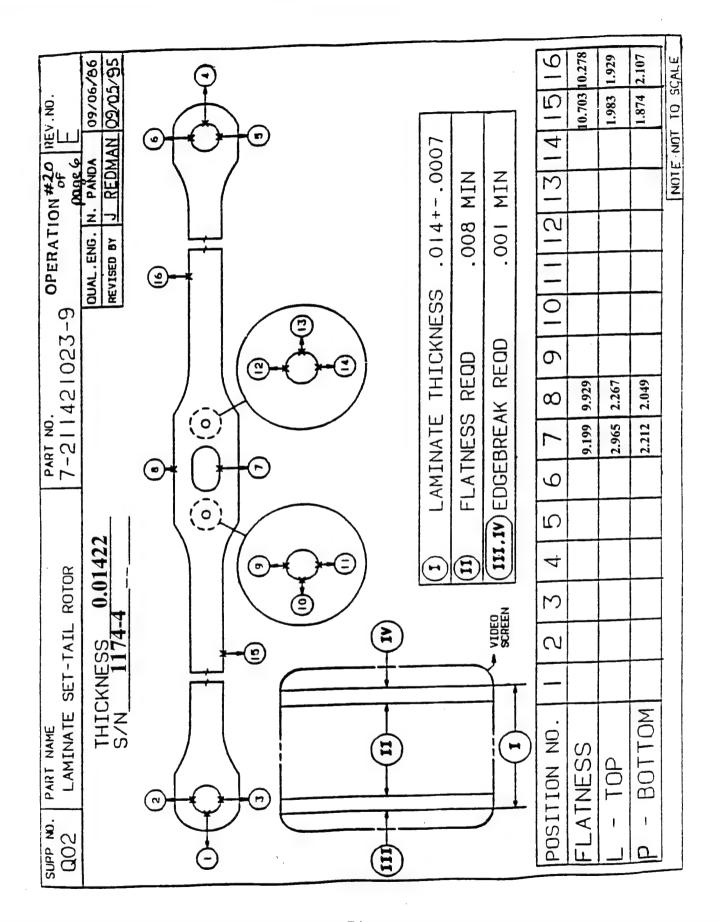
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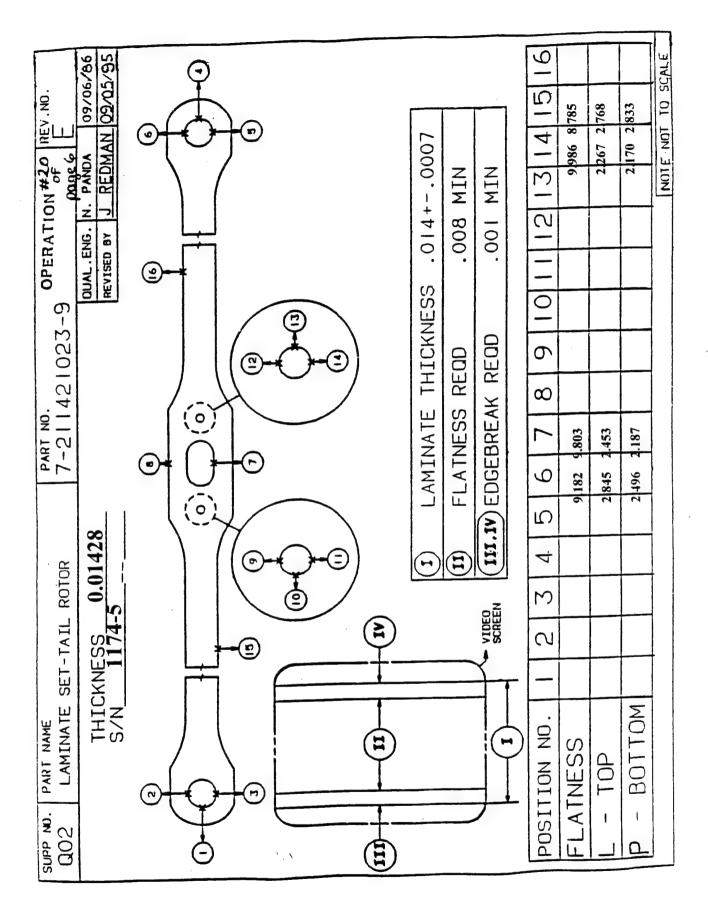
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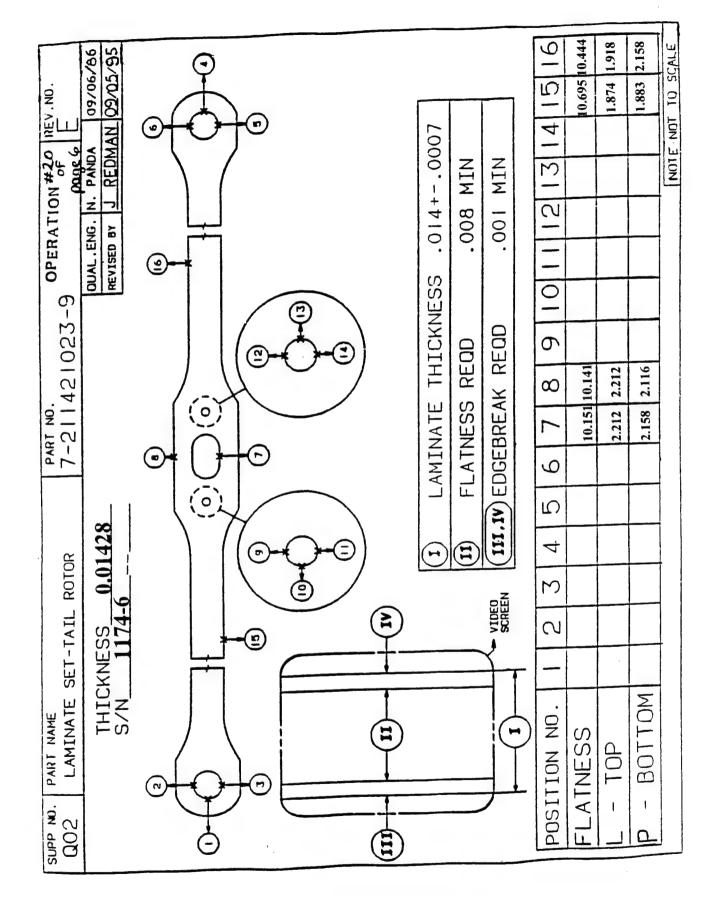


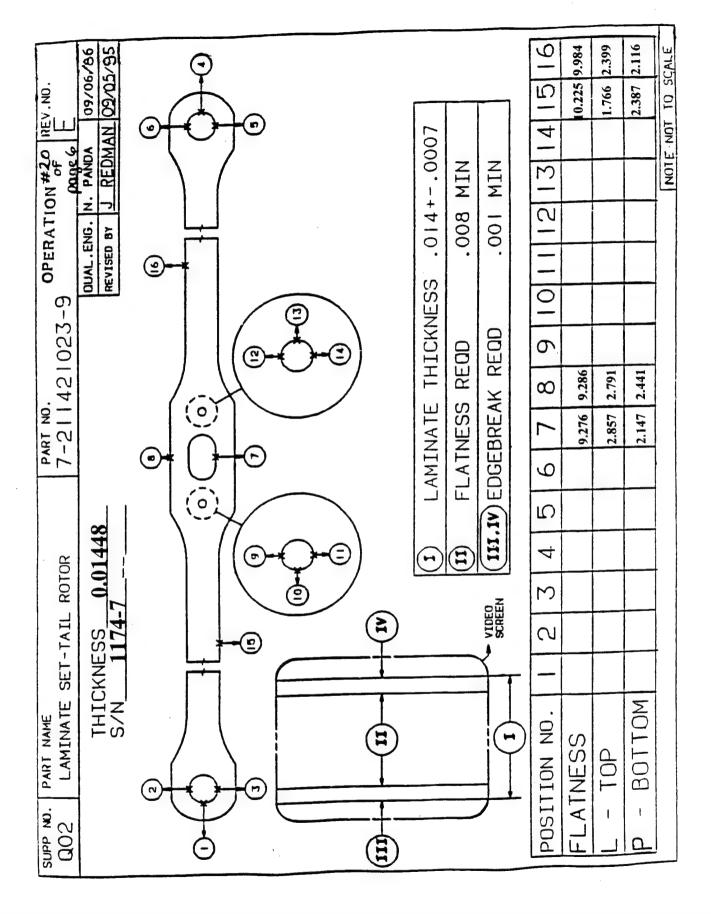


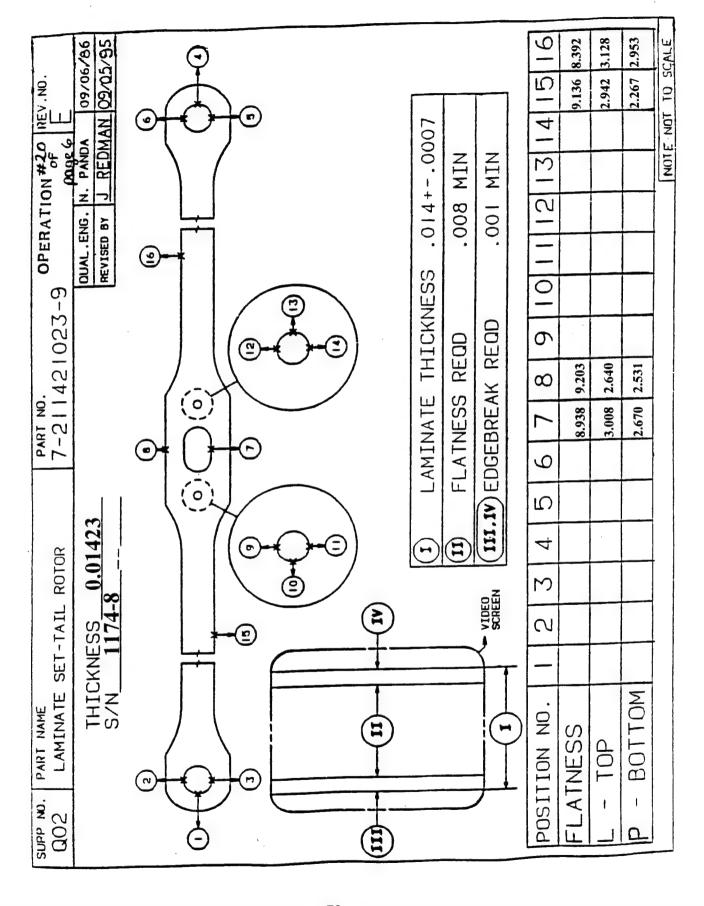


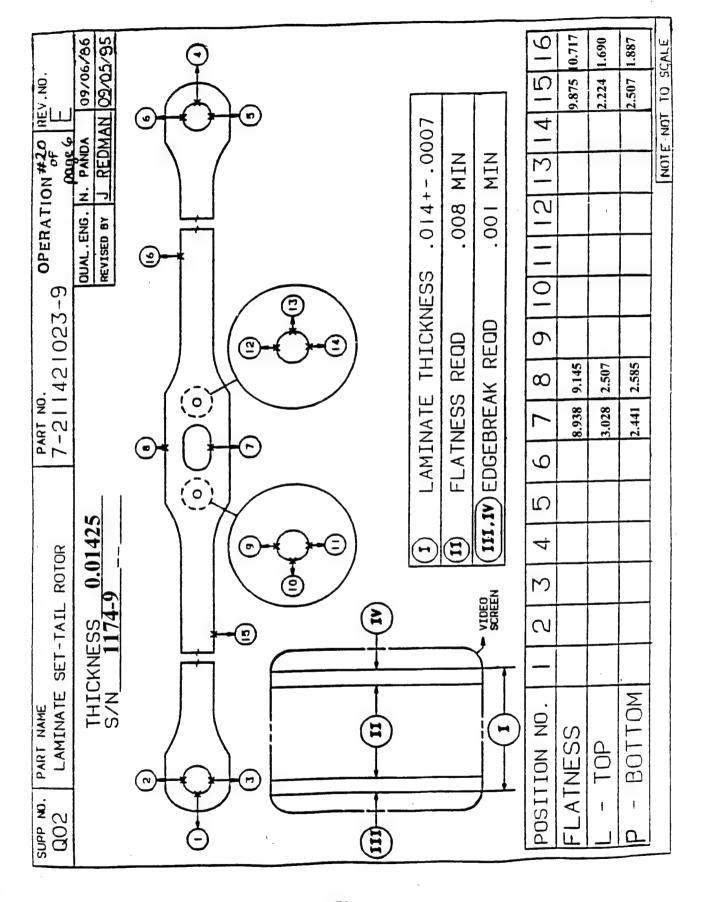


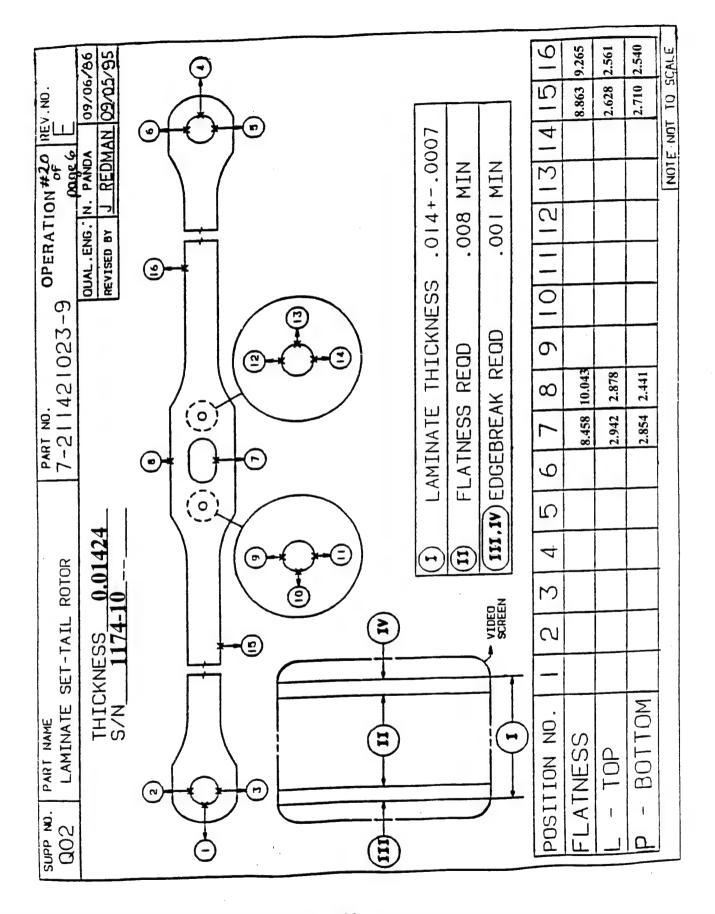


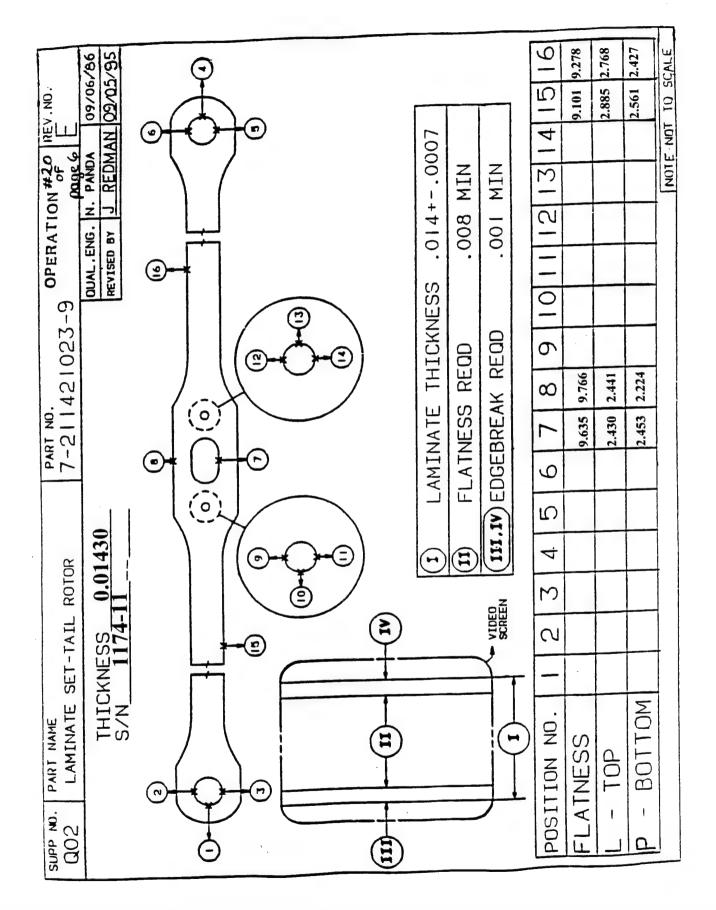


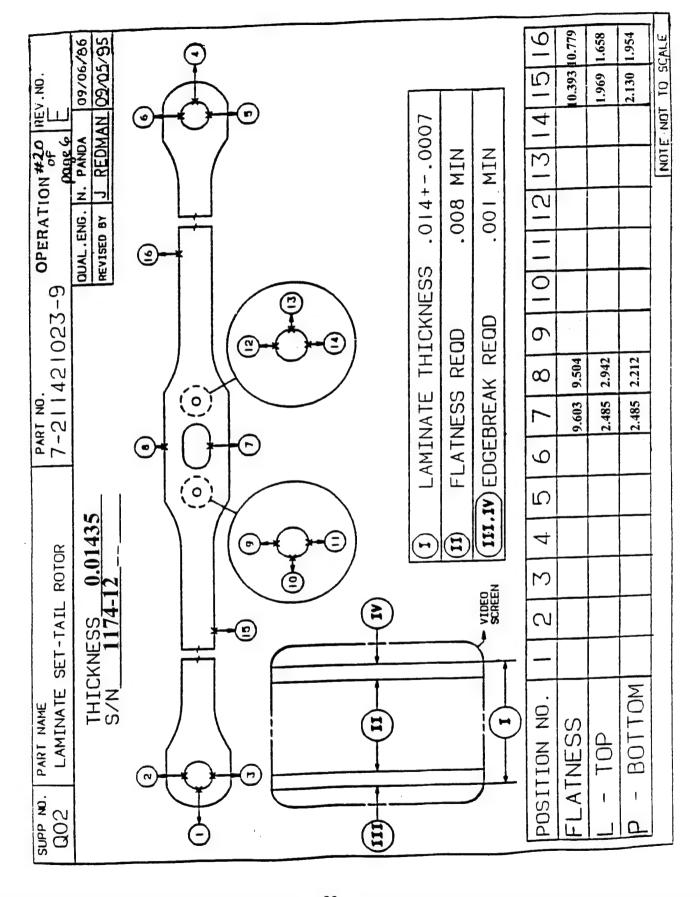


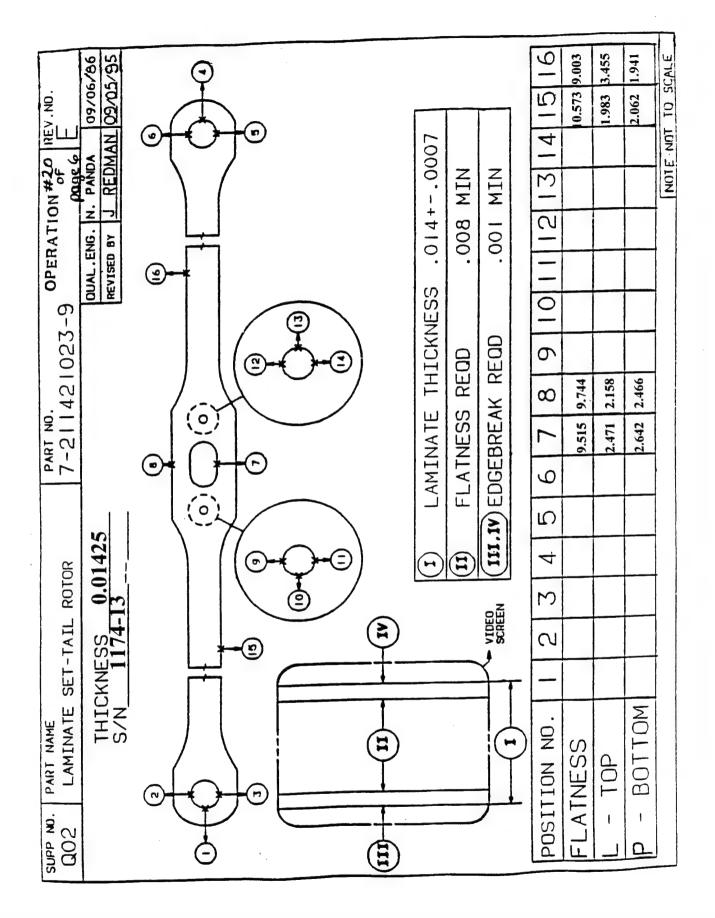


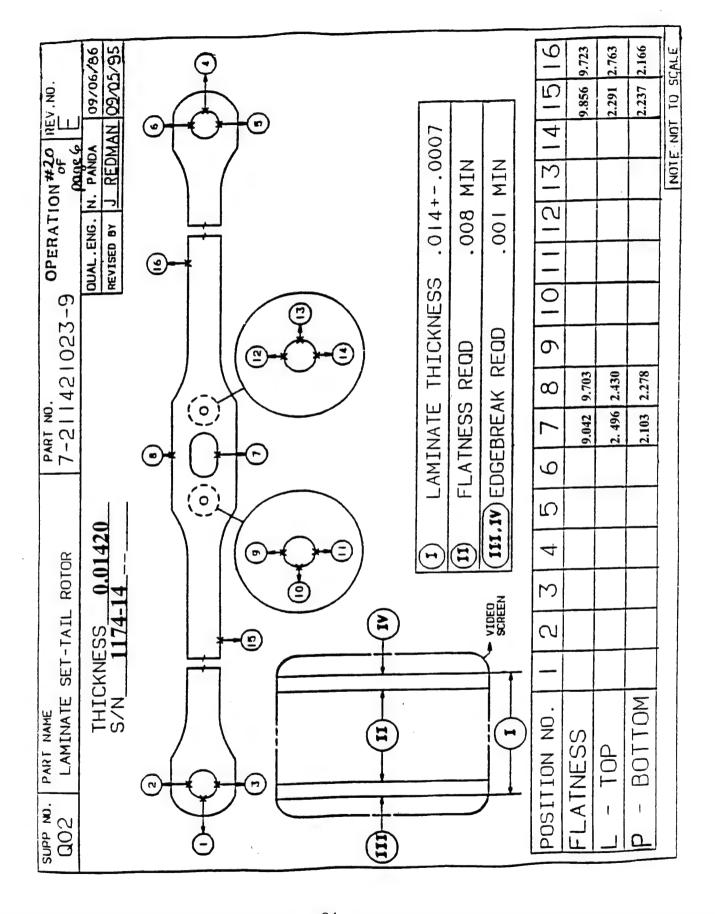


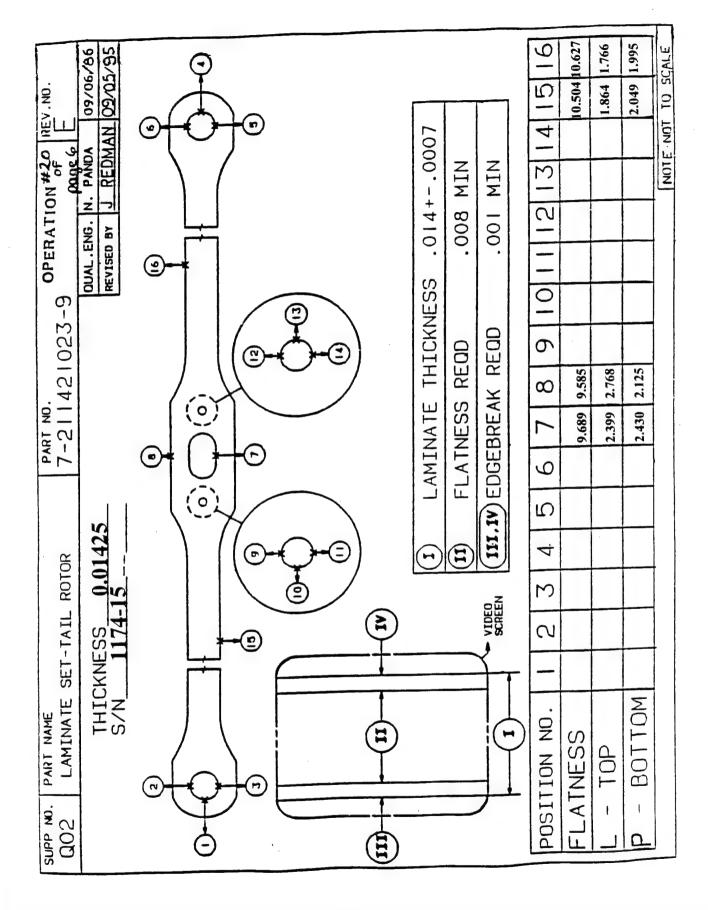


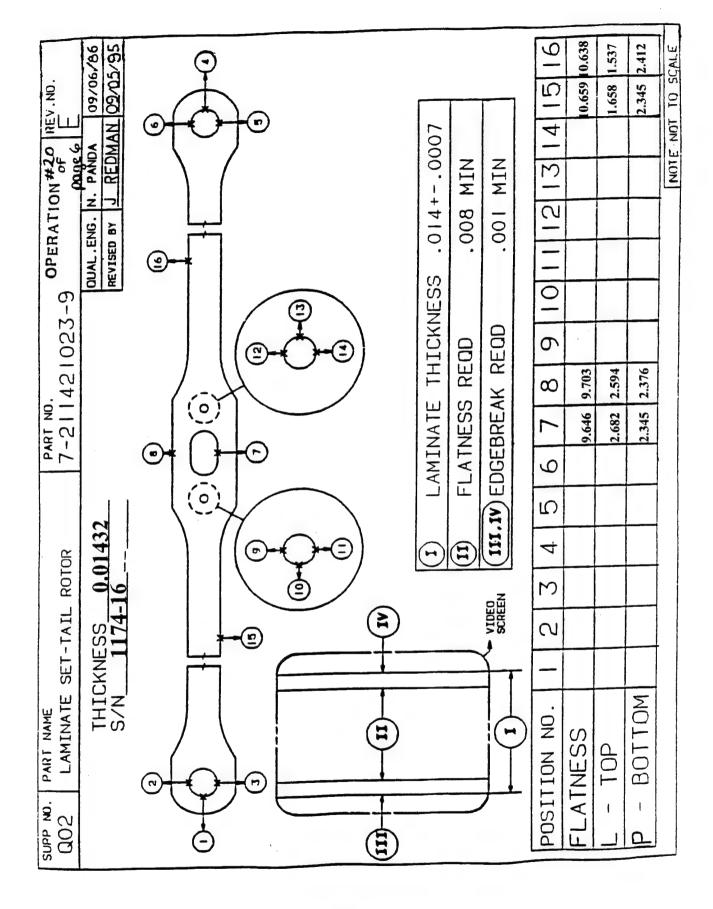


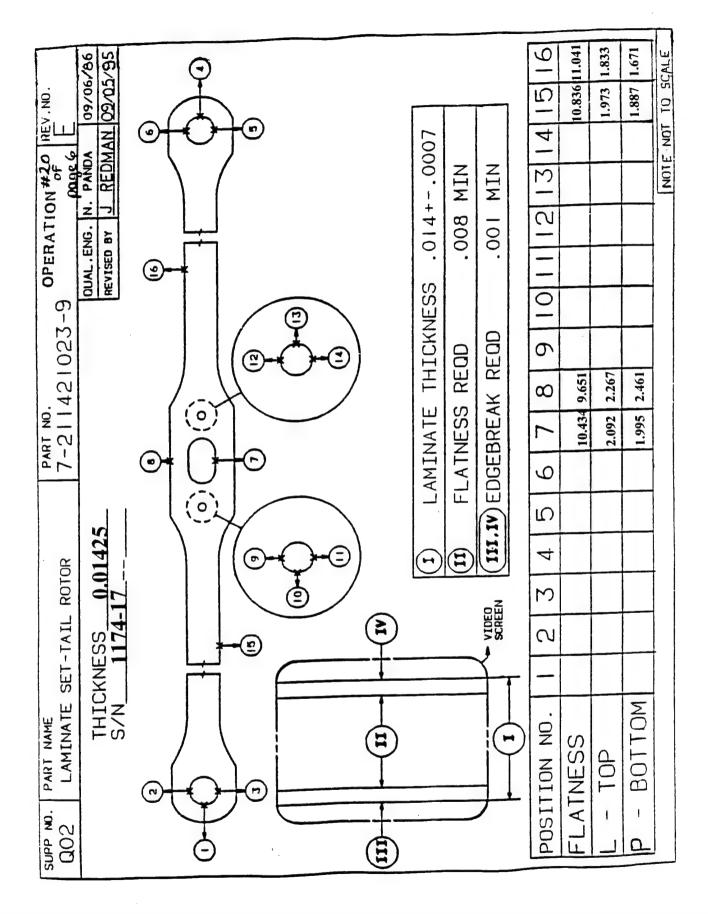


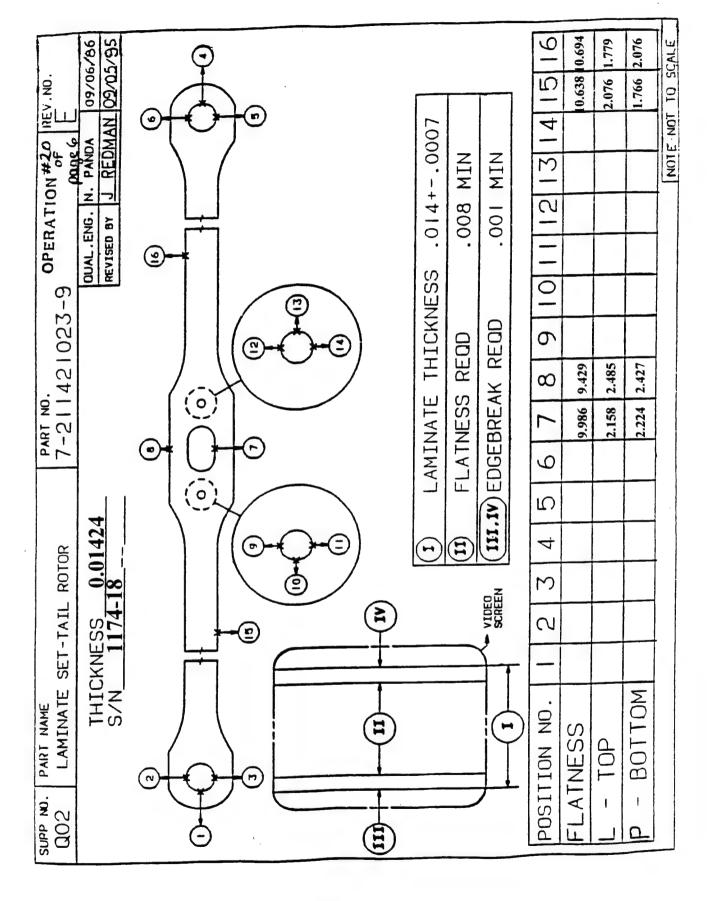


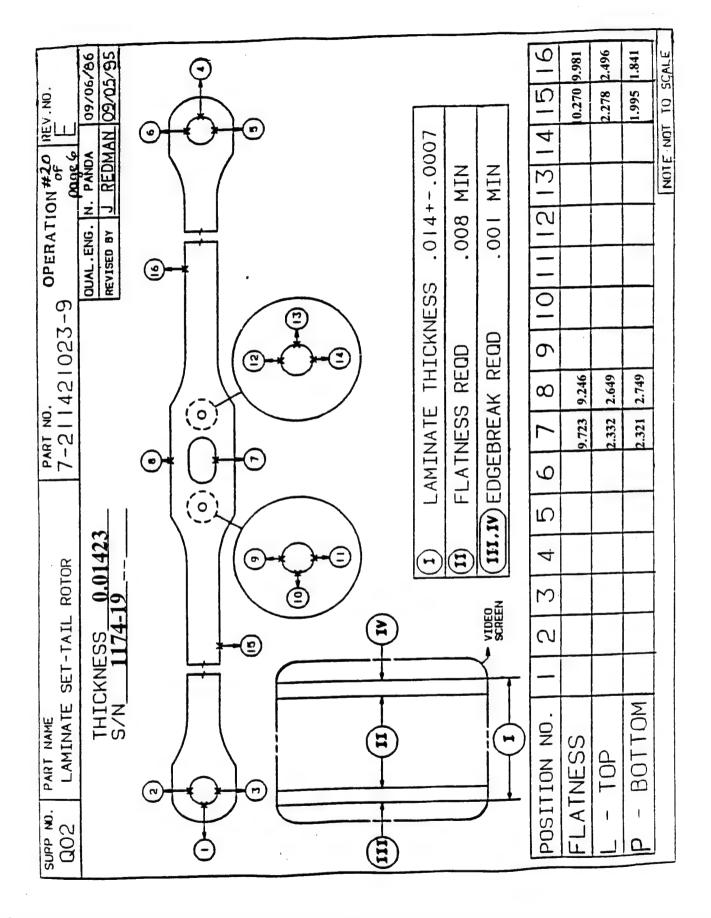


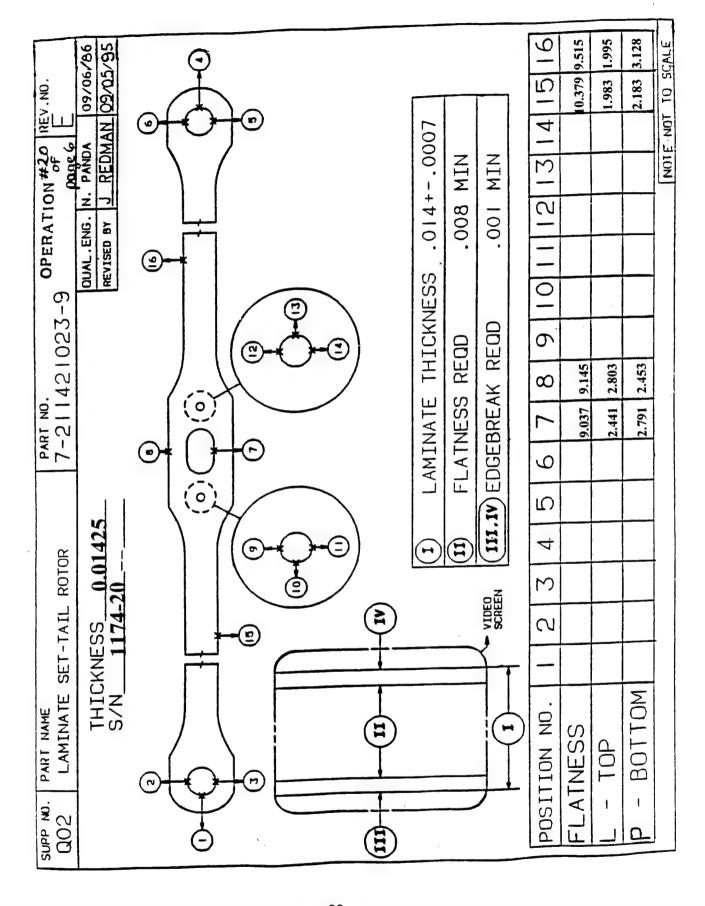


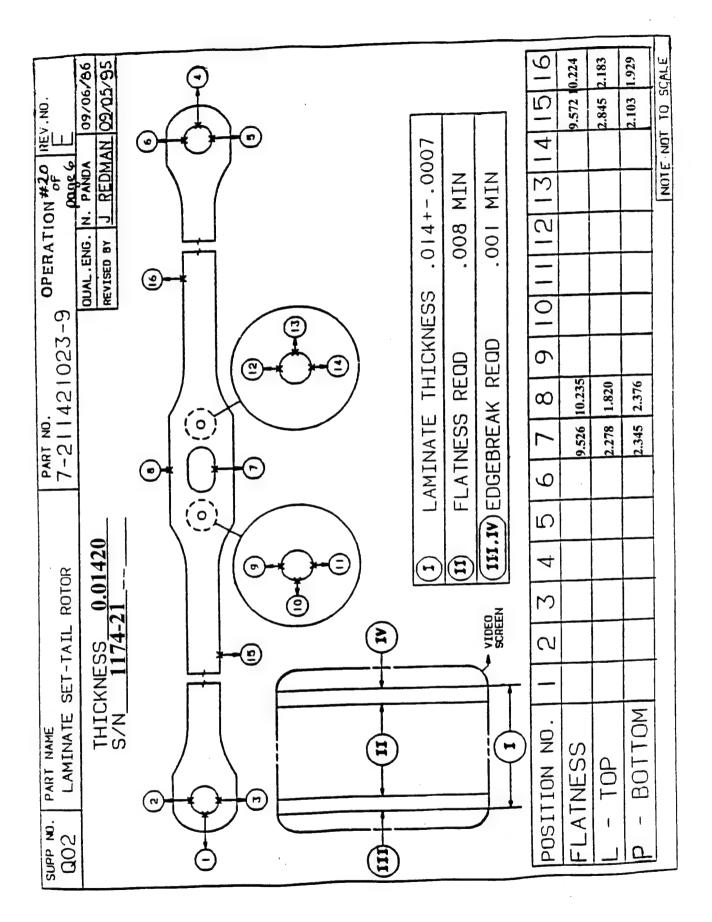


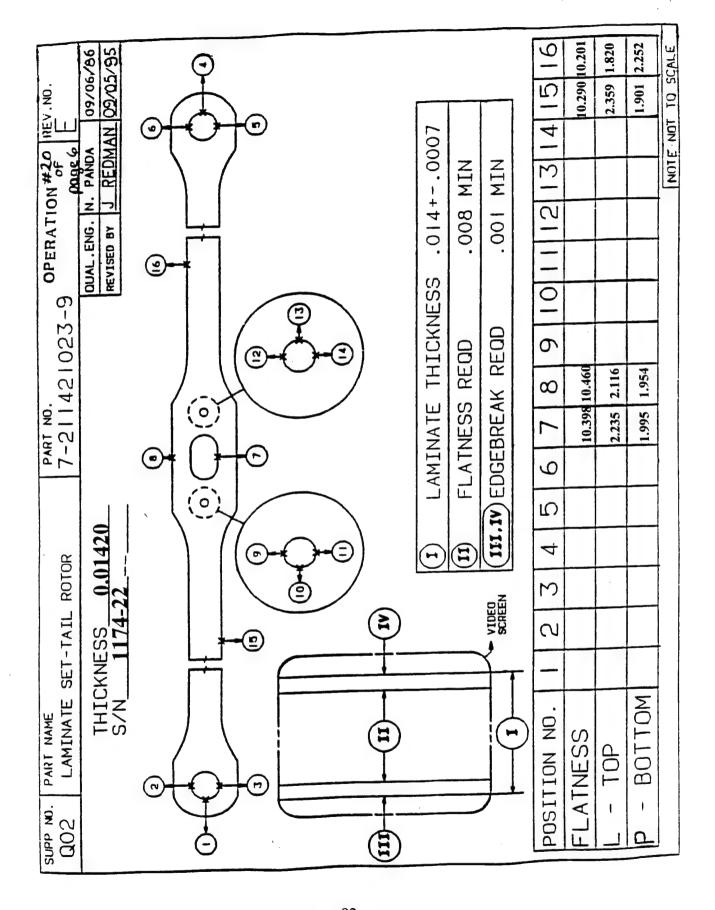








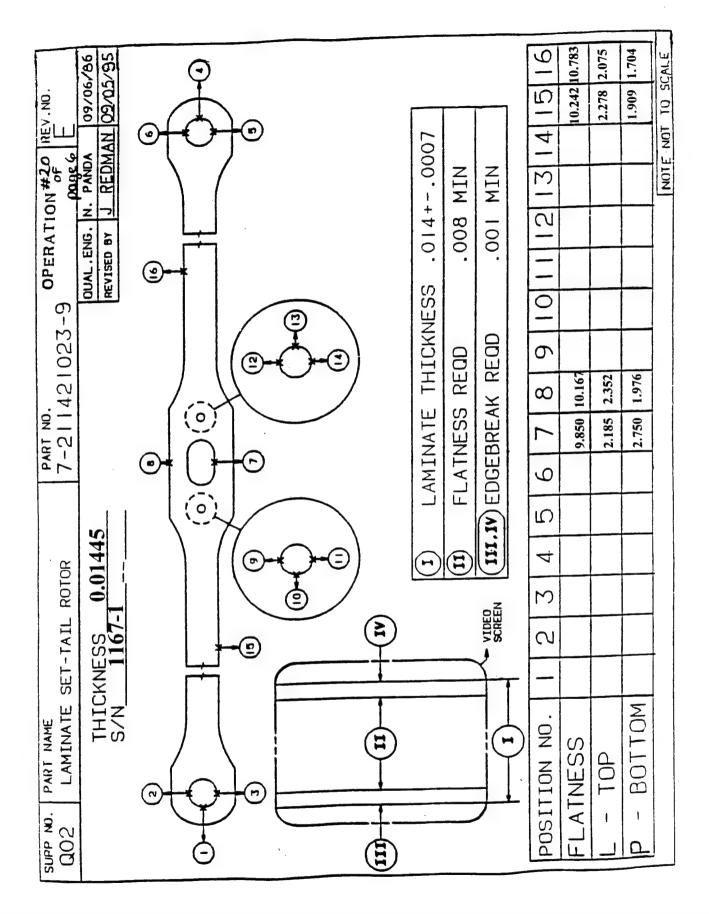


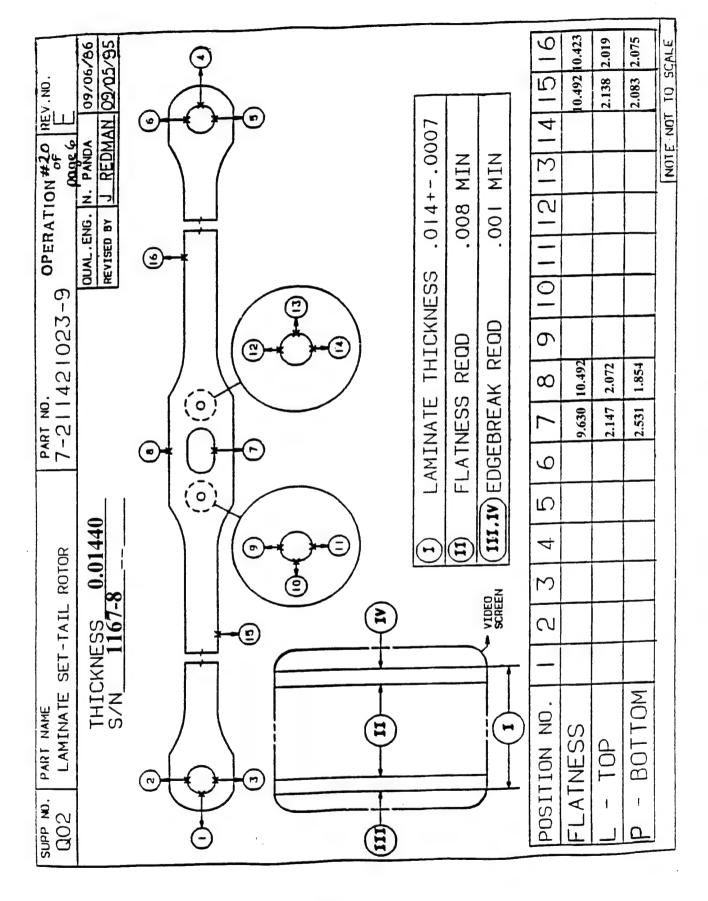


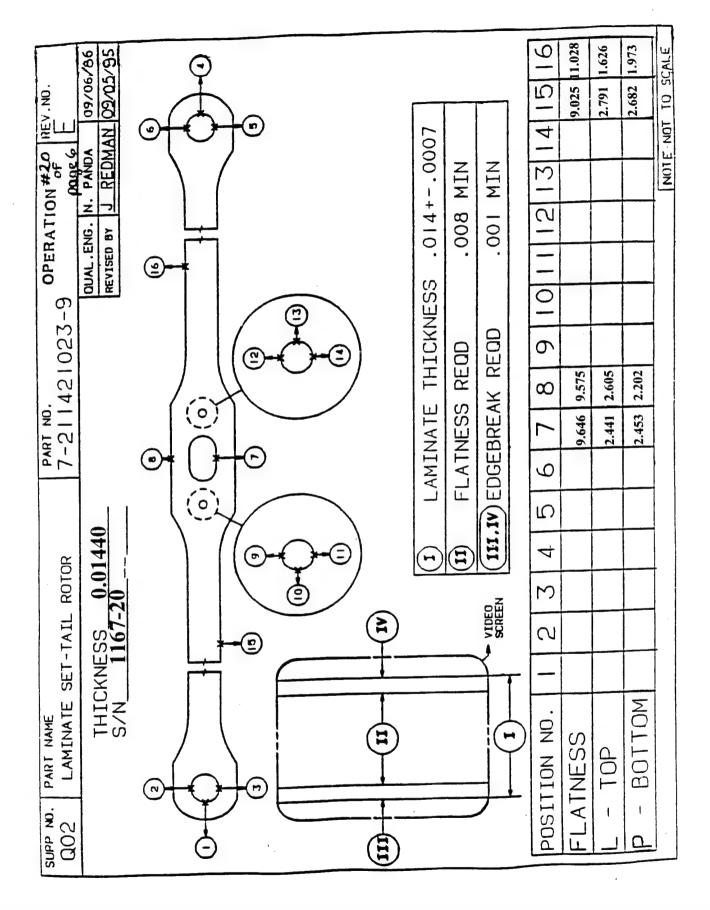
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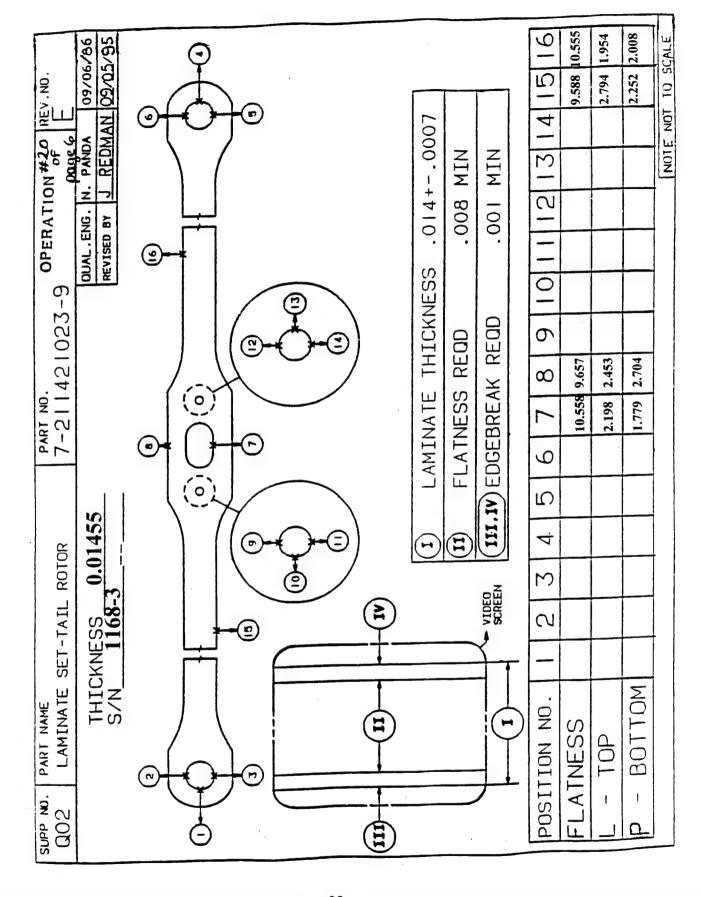
Edge Break Data for Randomly Selected
Strap Pack Laminates
From Packs 1167–1177 and Two "Extra" Laminates

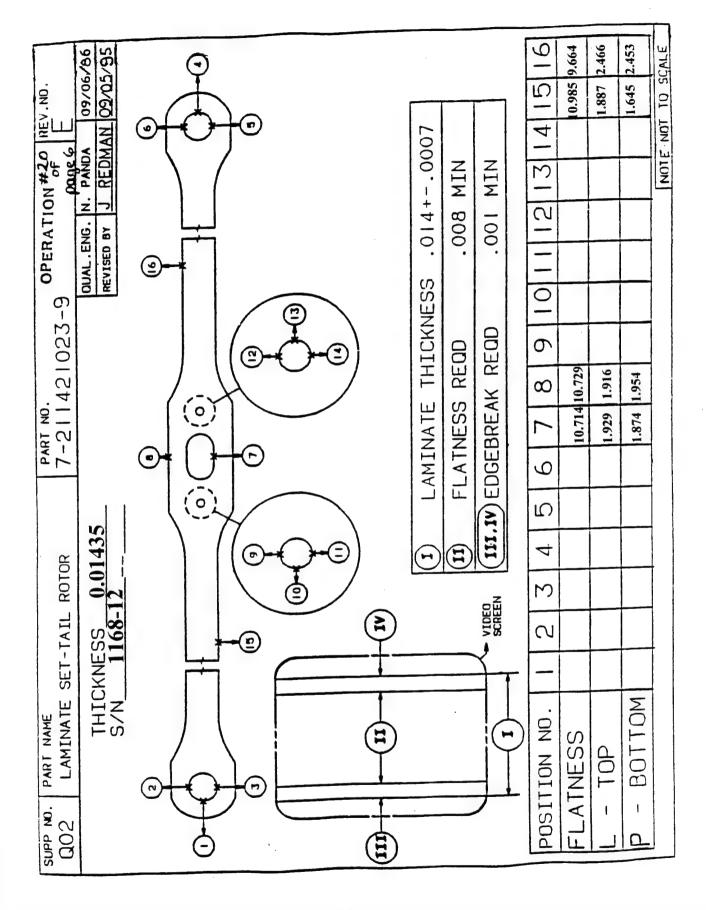
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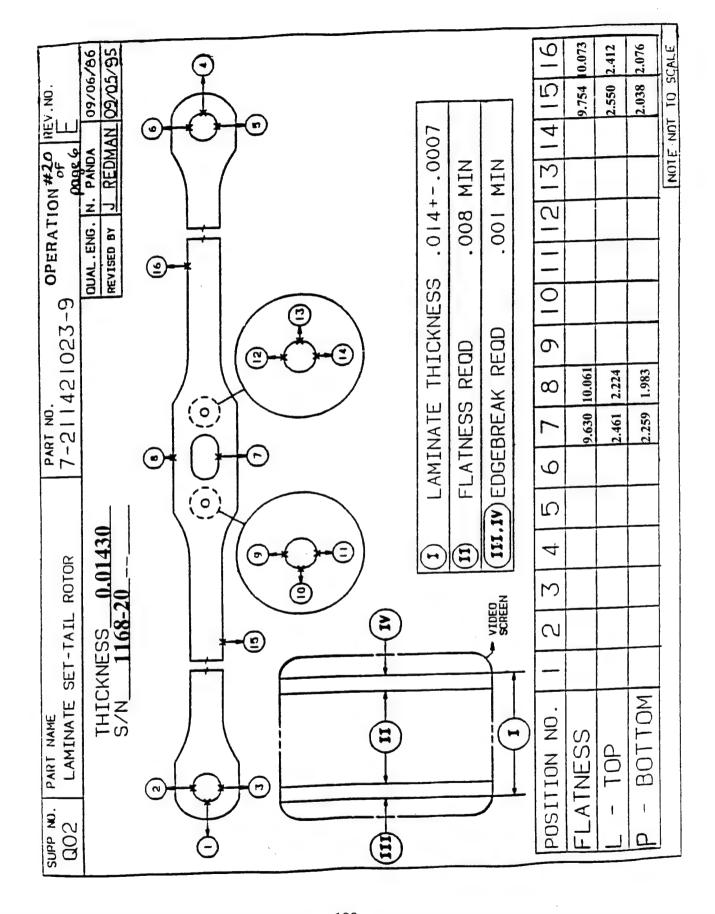


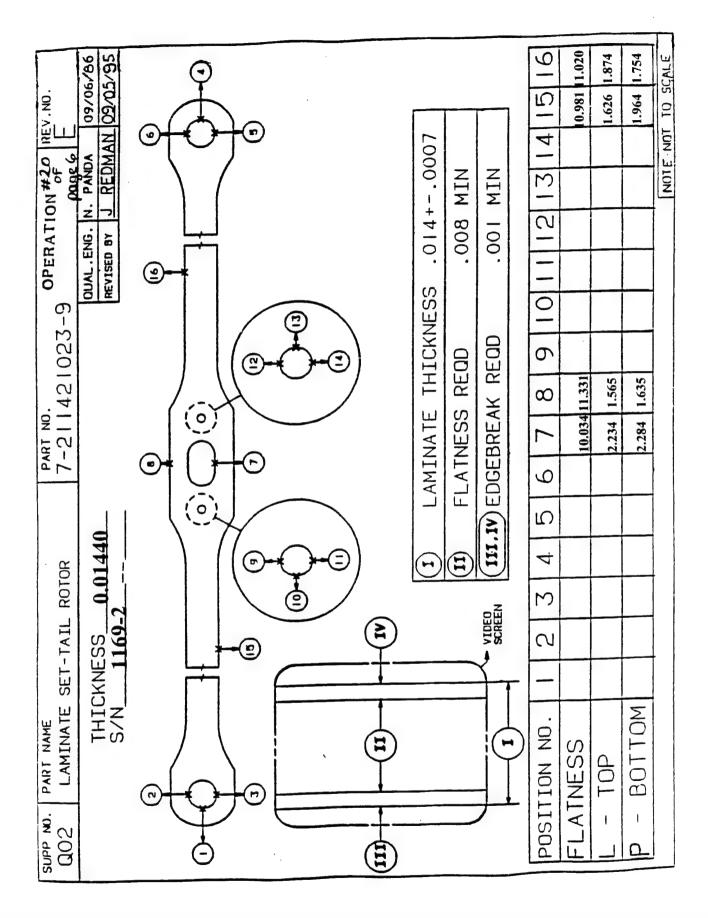


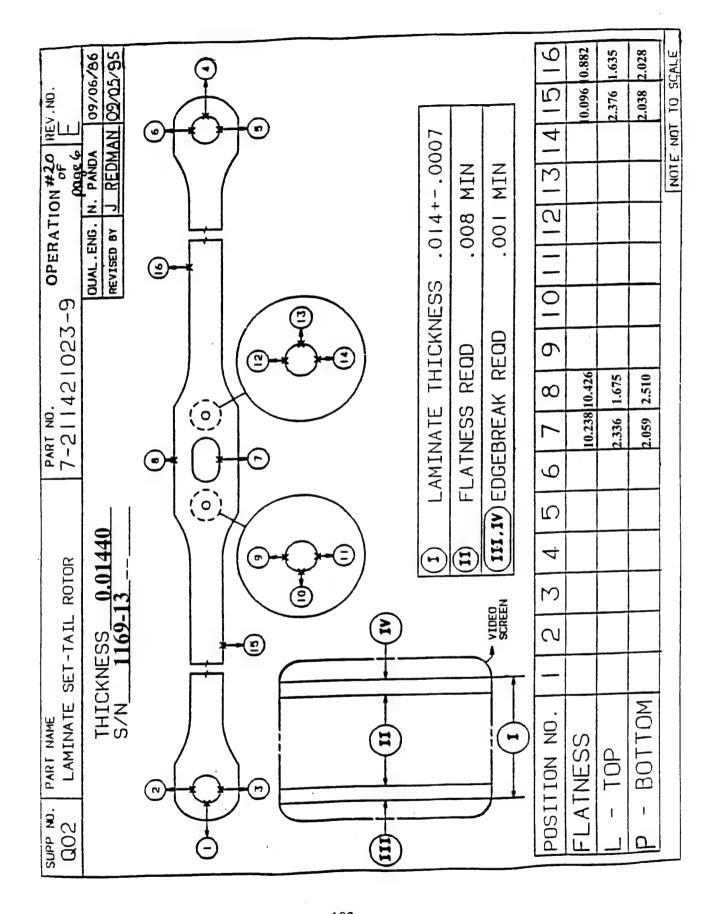


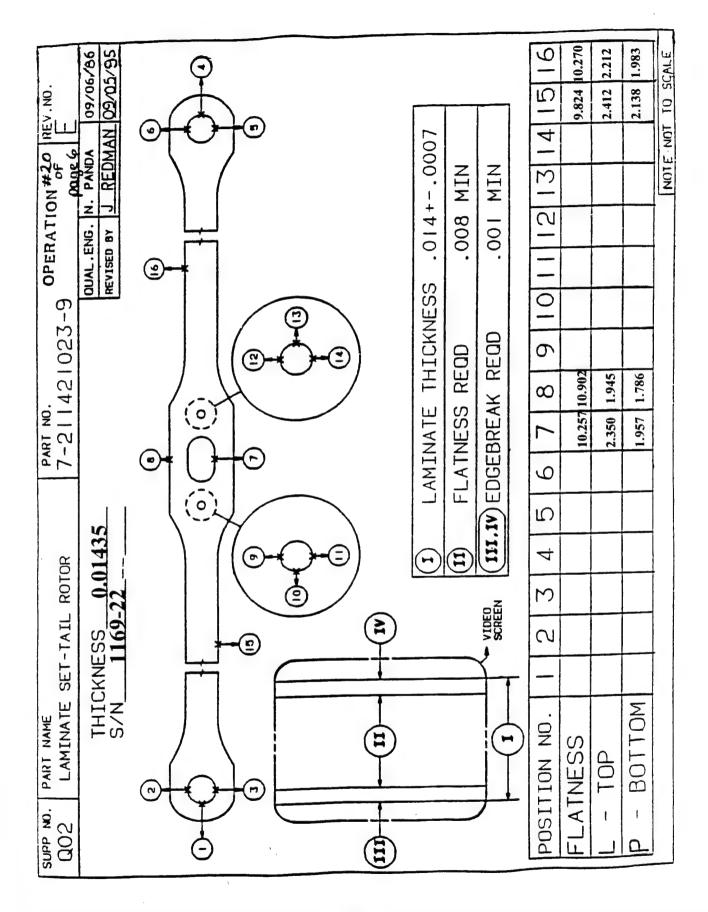


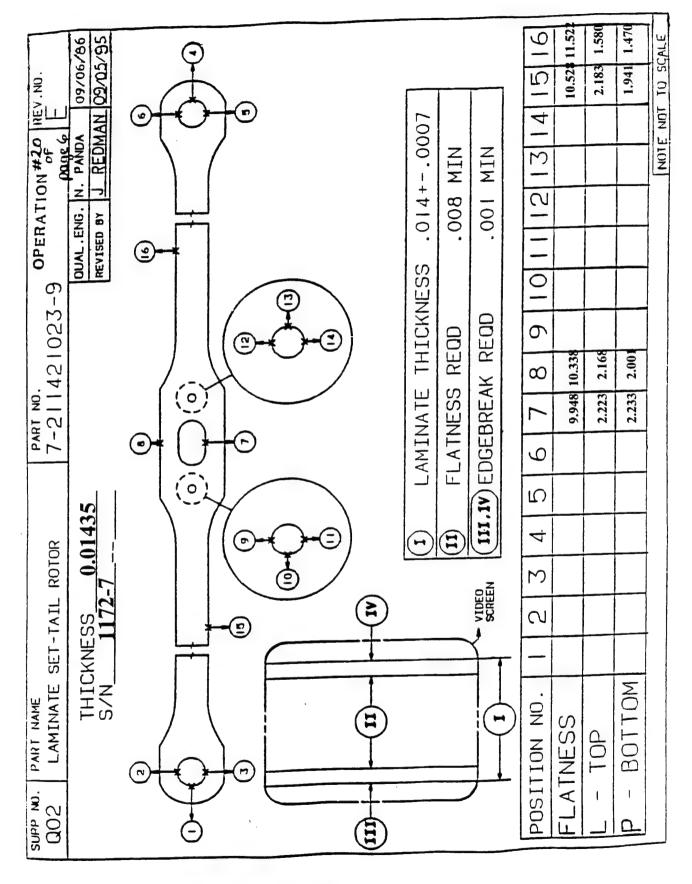


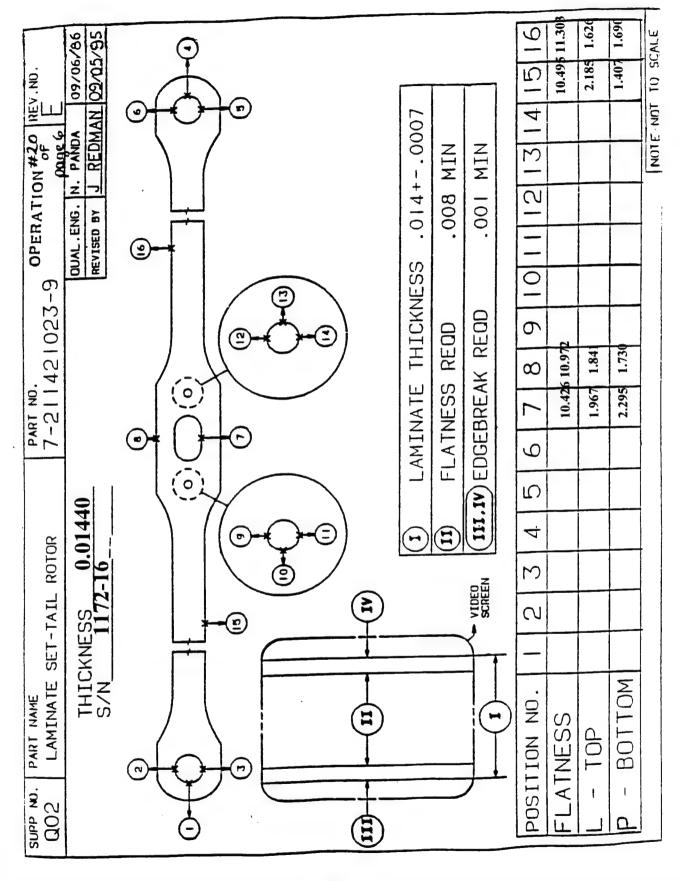


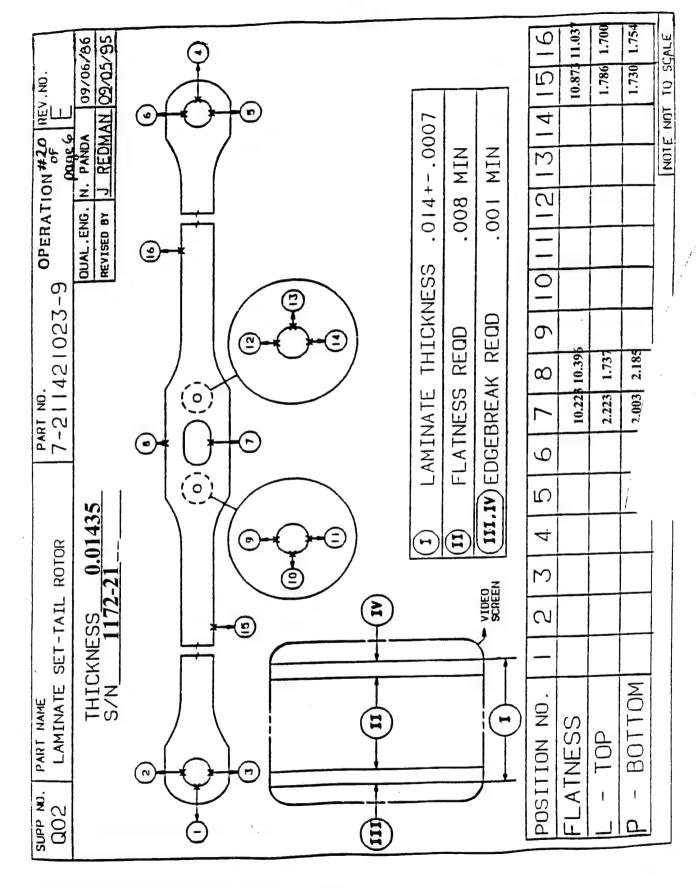


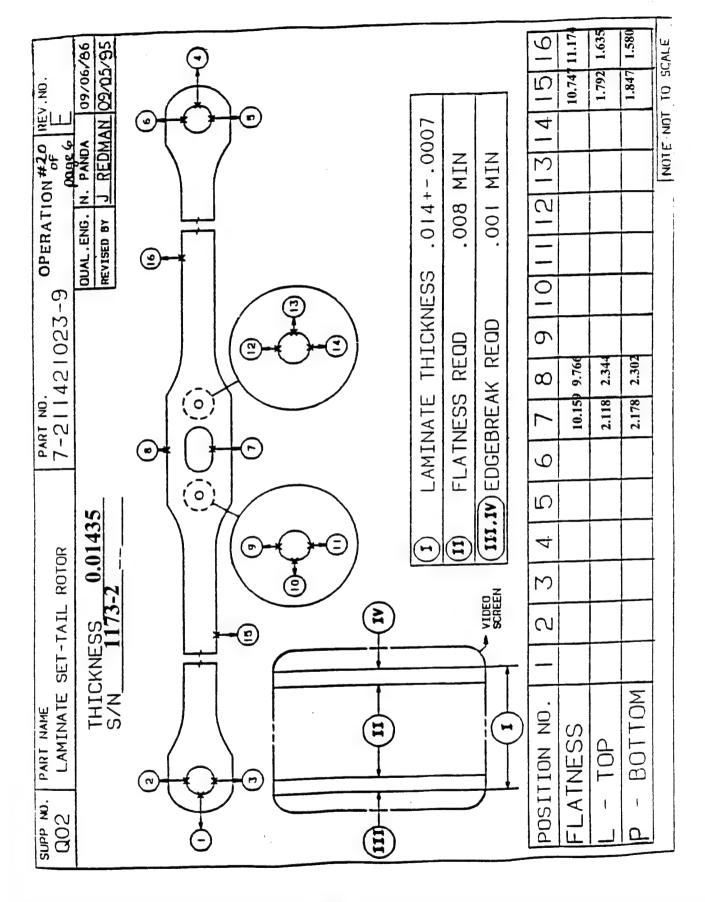


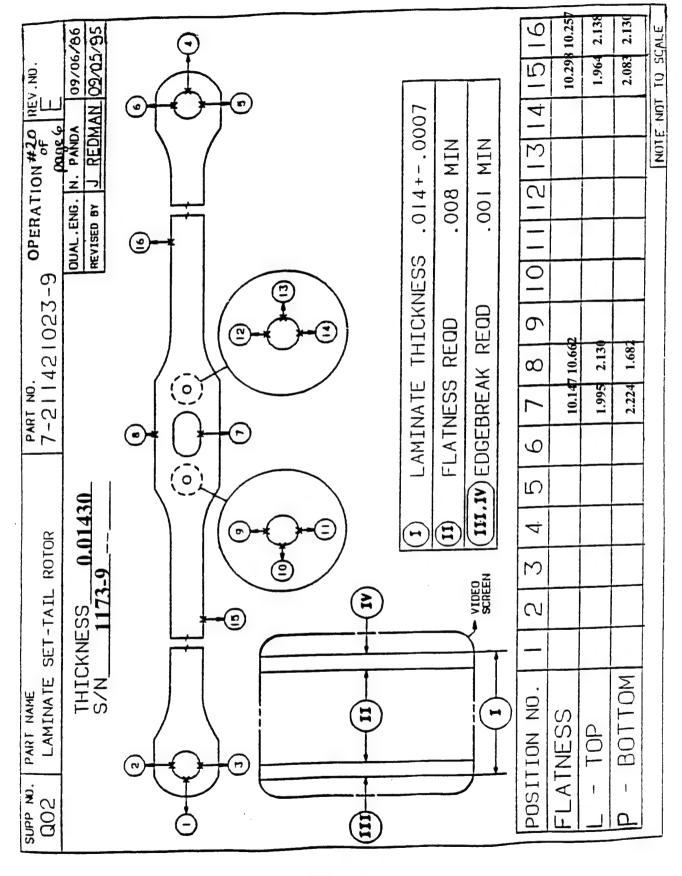


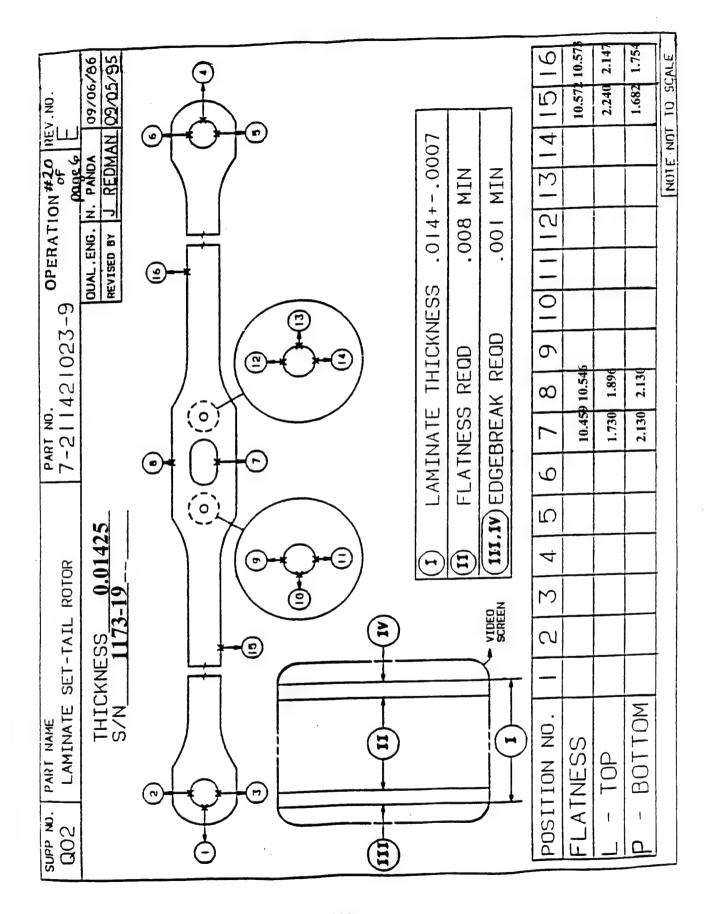


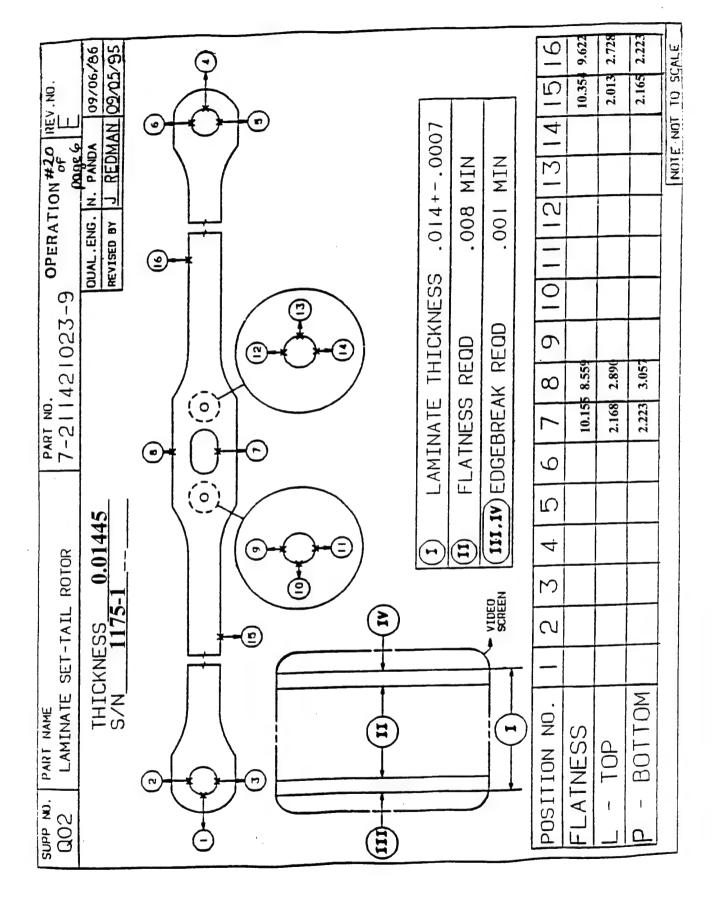


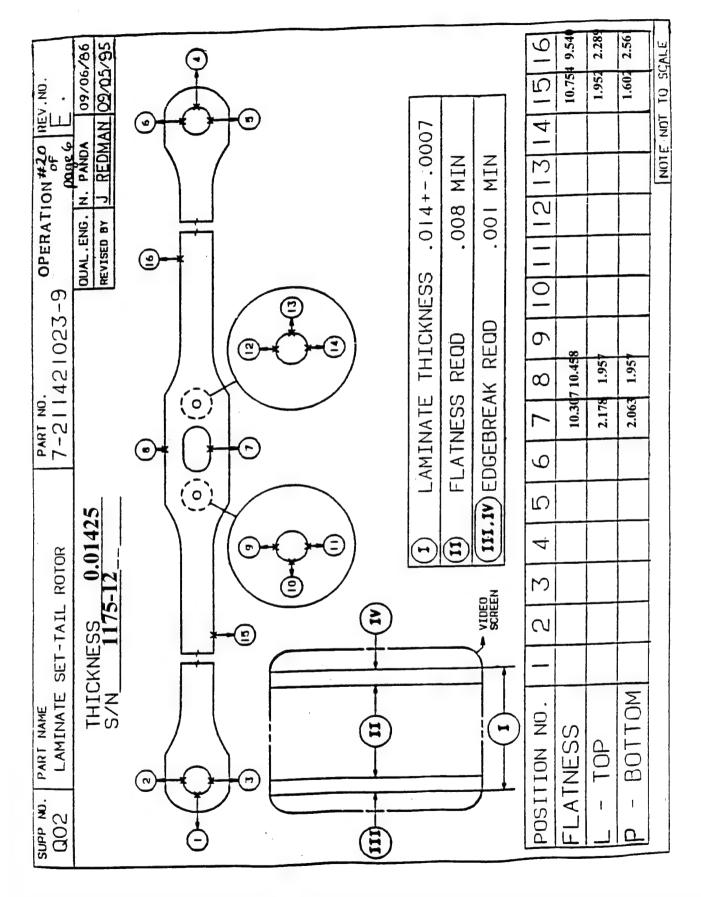


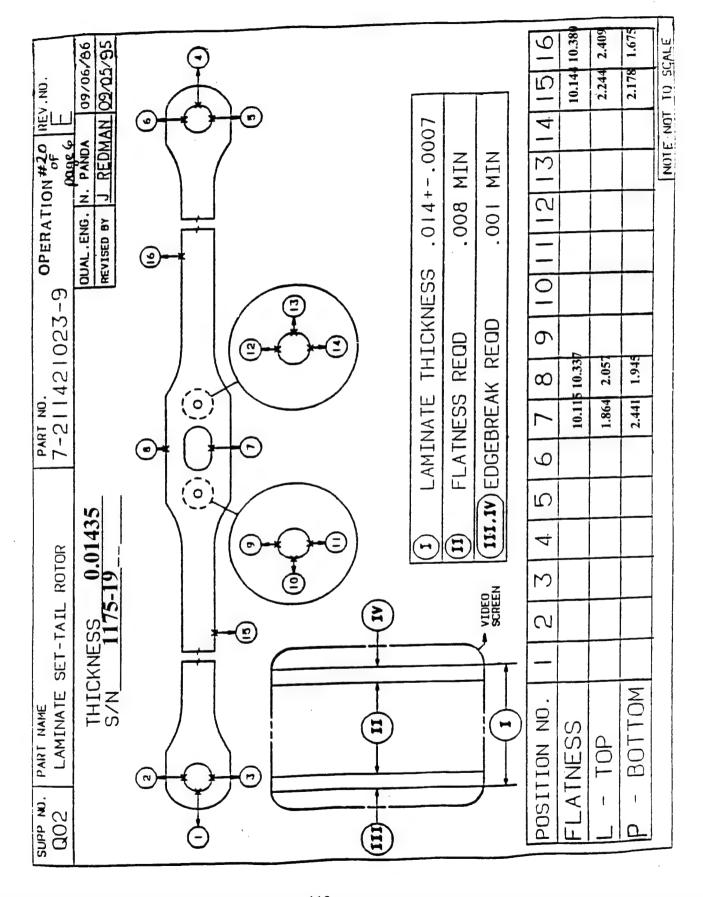


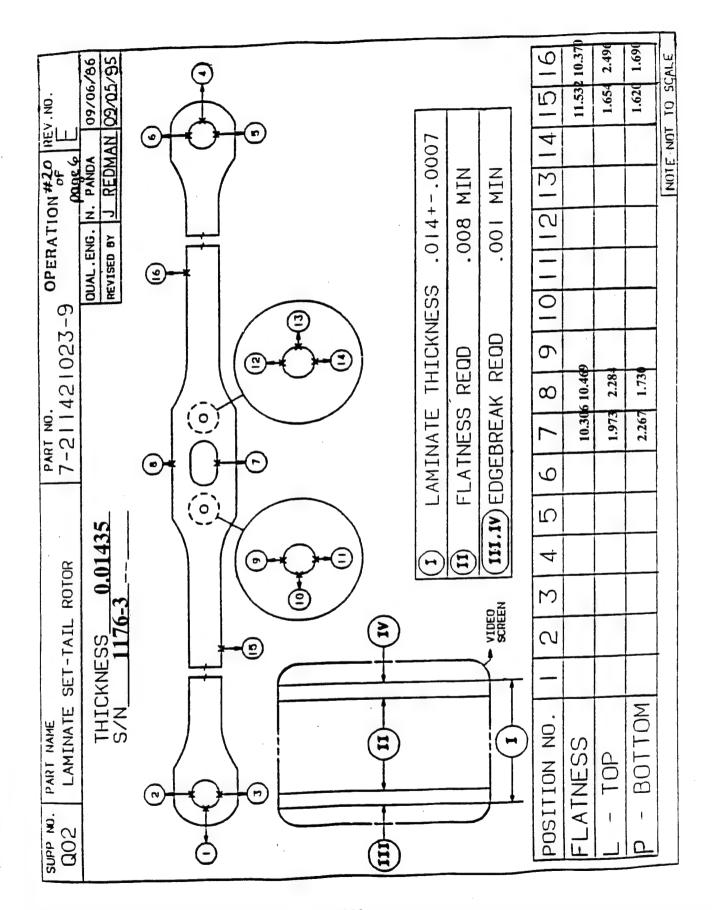


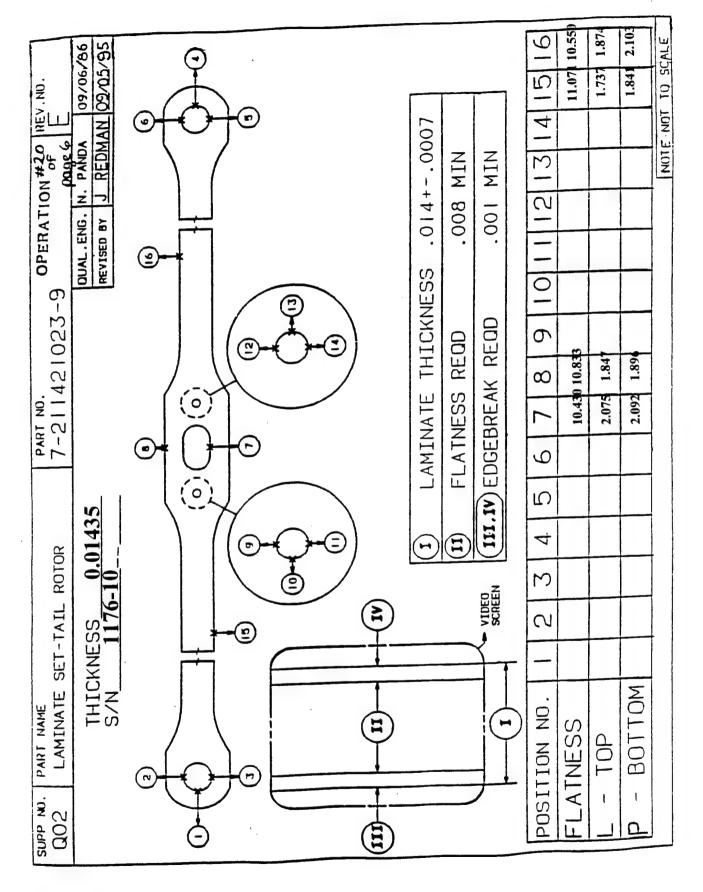


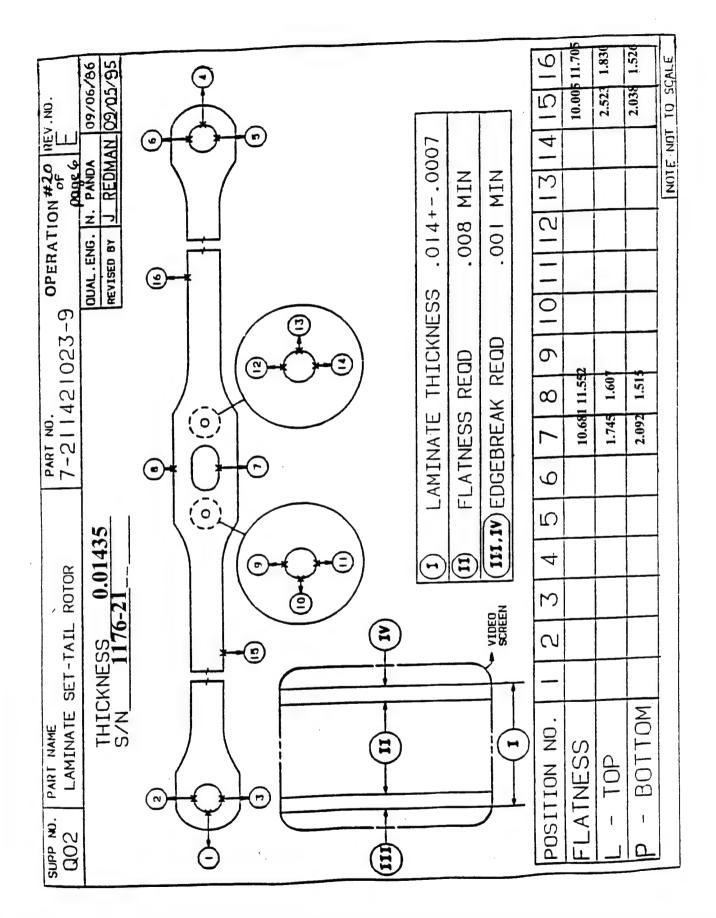


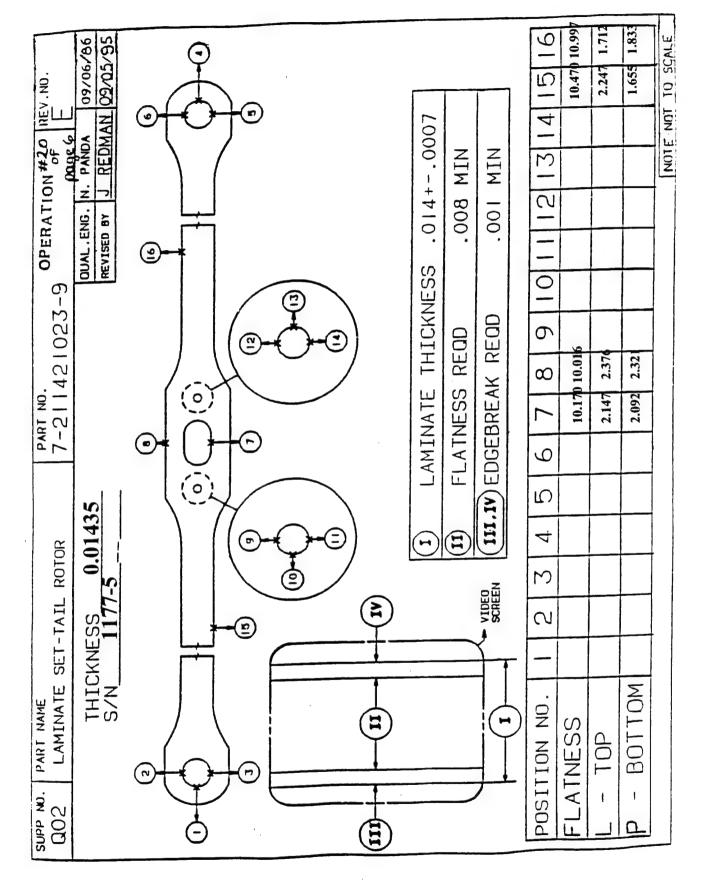


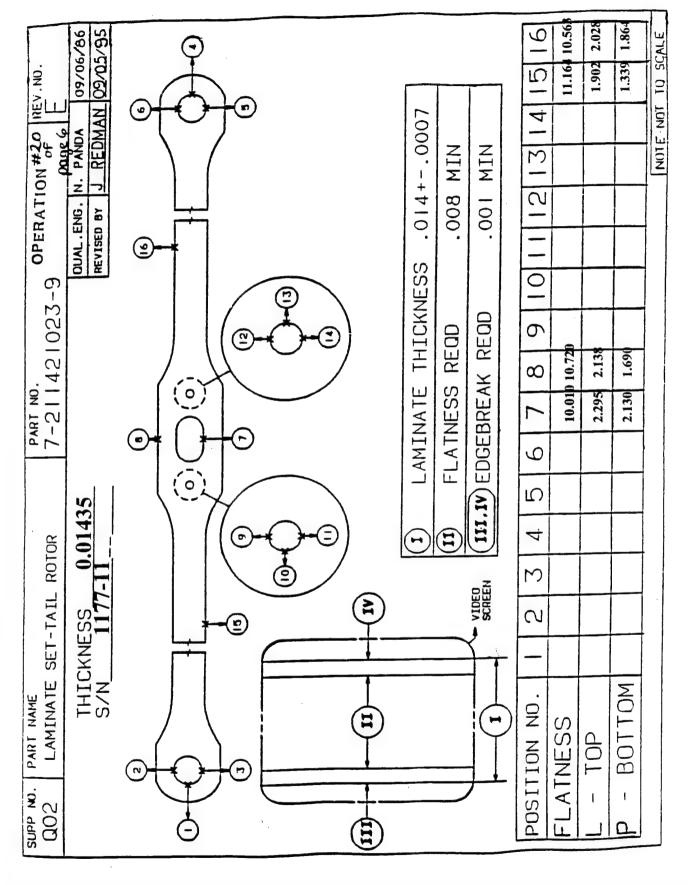


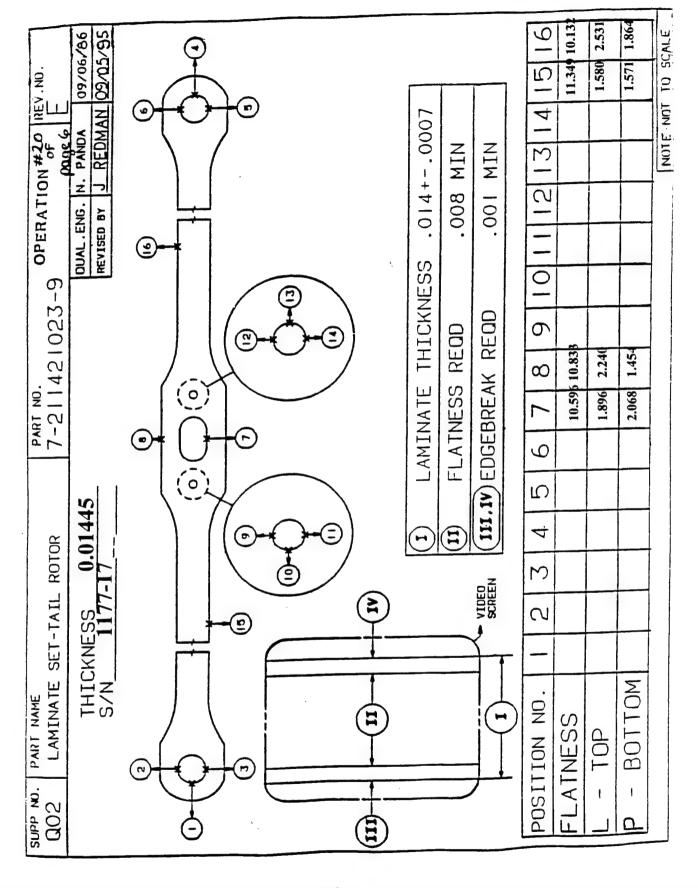


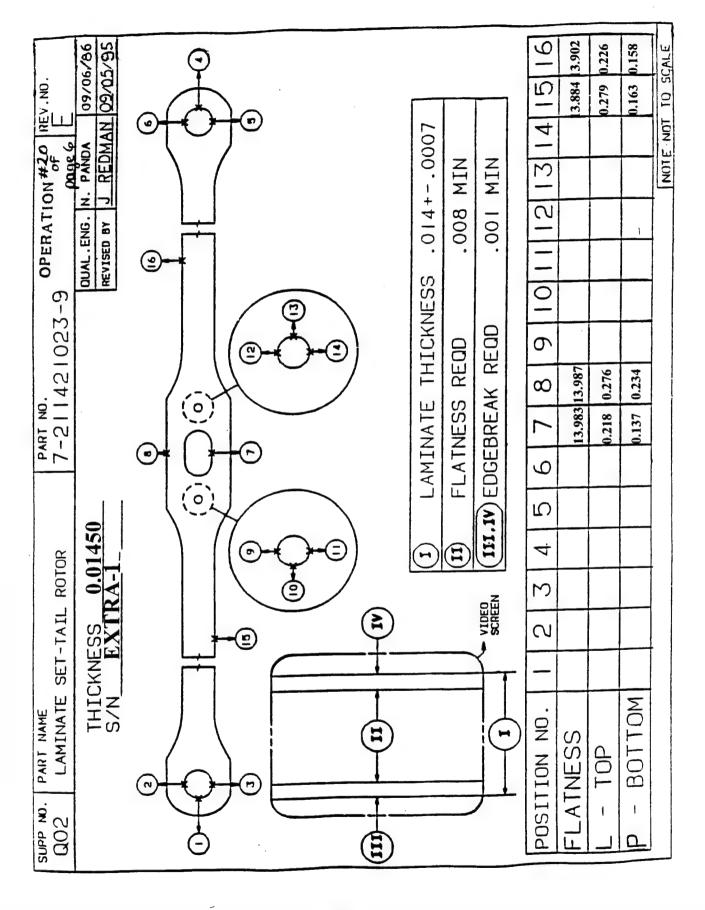


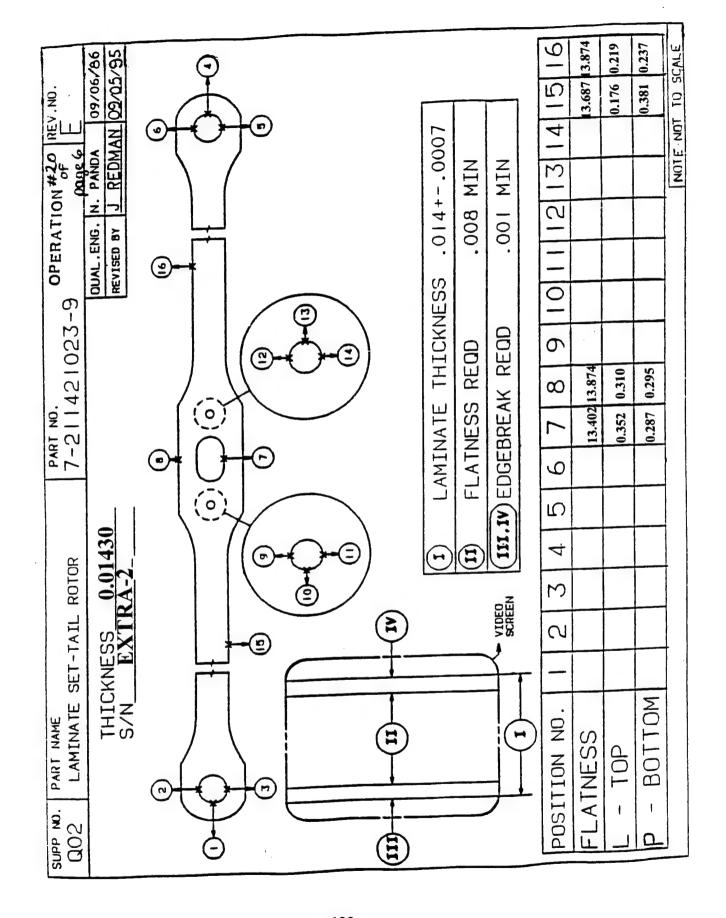












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13. ABSTRACT (Maximum 200 words)

The U.S. Army Research Laboratory-Weapons and Materials Research Directorate (ARL-WMRD) performed a dimensional inspection and metallurgical investigation of AH-64 Apache tail rotor strap pack assemblies and individual laminate sets. All of the dimensional critical characteristics were examined in an attempt to determine the cause of a buckling phenomenon within the strap pack assemblies. Conformance to the manufacturer's governing specifications with respect to the material, heat treatment, and marking requirements was also investigated. The cause of the buckling was attributed to a combination of factors. Dimensional nonconformances were identified. Most of the hole diameters were found to be well below the specified range, causing the assemblies to be forced together. Transposition of the laminates during manufacture was also highly likely to have occurred, adding to the misalignment of the assembly. All other characteristics of the laminates and assemblies were found to conform to the governing part drawings and specifications.

14. SUBJECT TERMS	15. NUMBER OF PAGES		
AM-355, dimensional inspection, strap pack, metallurgy			124
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